



Project Number: U2716-072-181

February 14, 2019

Sunmodo
14800 NE 65th Street
Vancouver, WA 98682

**REFERENCE: British Columbia Ground Mount
Ground Mount PV Array Installation**

To Whom It May Concern:

Per request of Sunmodo, we have been asked to prepare the structural design of a ground-mounted PV solar array system with several foundation options as shown in the attached calculations. The adopted building code in this jurisdiction is the British Columbia Building Code 2018. Vector Structural Engineering requires that we or another licensed engineer review each site specific install, and we are not liable for installs at site specific locations we have not reviewed. Because the British Columbia Building Code does not address the wind effects on open structures, the following design parameters are used in our analysis:

- Minimum Design Loads for Buildings and Other Structures (ASCE 7-10)
- Design wind speed for risk category I structures: 105 mph (46.9 m/s) (3-sec gust)
- Wind exposure: C
- Ground snow load: 68.9 psf (3.3 kPa)
- The ground screws and helical piers must be tested to 1.5 times uplift and 2.0 times lateral reactions found in the table below.

Load (ASD)	Value (lbs / kN)	Factor of Safety	Test Value (lbs / kN)
UPLIFT	2400 / 10.7	1.5	3600 / 16.0
LATERAL	1900 / 8.5	2	3800 / 16.9

Foundation concrete shall have a minimum compressive strength of 3000 psi (20.7 MPa) at 28 days. Cement for all concrete shall be Type I or II with a minimum of 6% entrained air with a water/cement ratio of 0.50. Maximum aggregate size shall be 3/4". Design is based on concrete strength of 2500 psi (17.2 MPa) thus no special inspection of concrete strength is required.

Footings are designed based on an allowable soil bearing pressure of 1500 psf (71.8 kPa) an allowable skin friction of 250 psf (12 kPa), an allowable lateral bearing pressure of 150 pcf (2403 kg/m³), and a coefficient of friction of 0.25. Vector Structural Engineering strongly recommends independent soils testing be performed by a licensed geotechnical engineer to verify the assumed soil parameters.

All ground mounts are to be installed per manufacturer's recommendations. The use of solar panel support span tables provided by the manufacturer is allowed only where the site conditions and solar panel configuration match the description of the span tables. Electrical engineering is beyond our scope. All work performed must be in accordance with accepted industry-wide methods and applicable safety standards. Vector Structural Engineering assumes no responsibility for improper installation of the solar panels.

Very truly yours,

VECTOR STRUCTURAL ENGINEERING, LLC

Russell Emery, P.E.
British Columbia License: 201804 - Expires: 12/31/2019
Project Engineer

RNE/stb

Enclosures

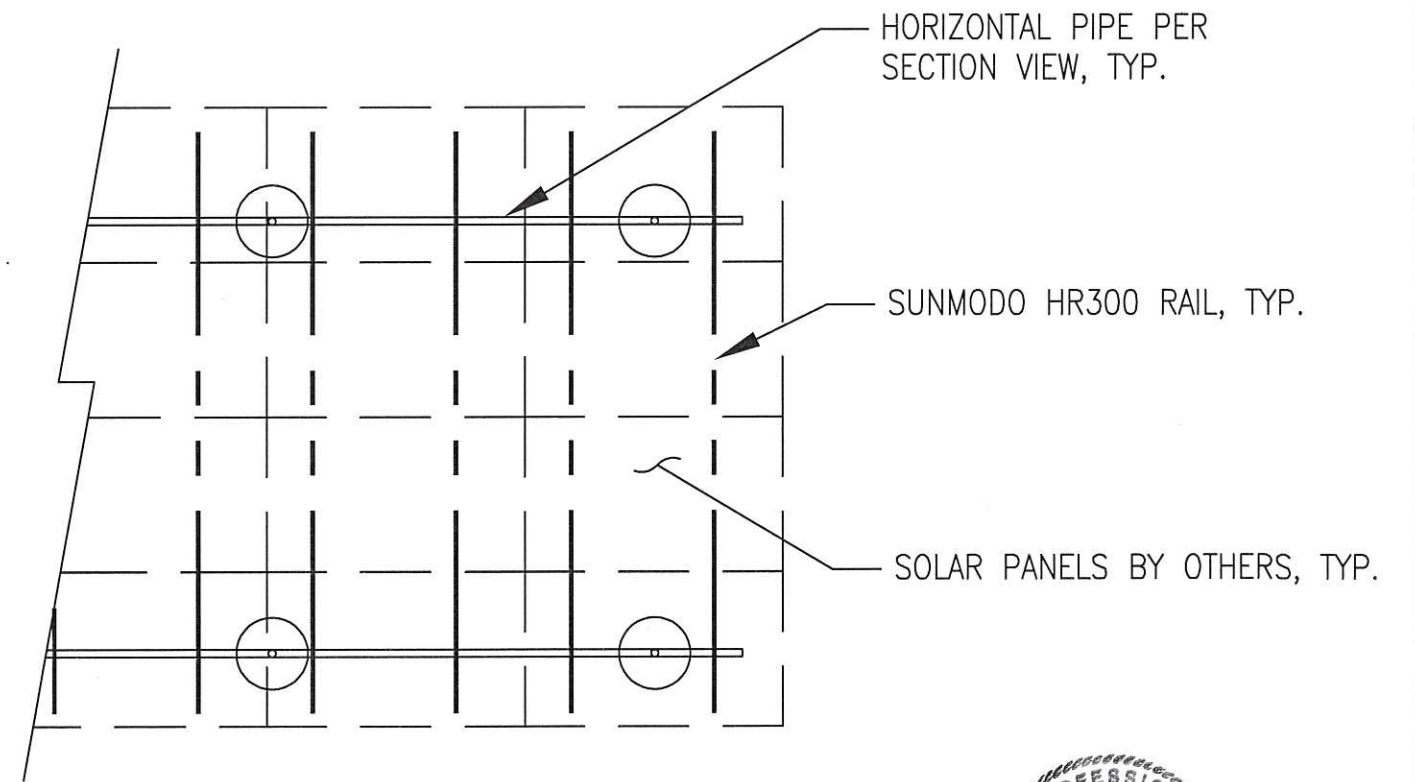
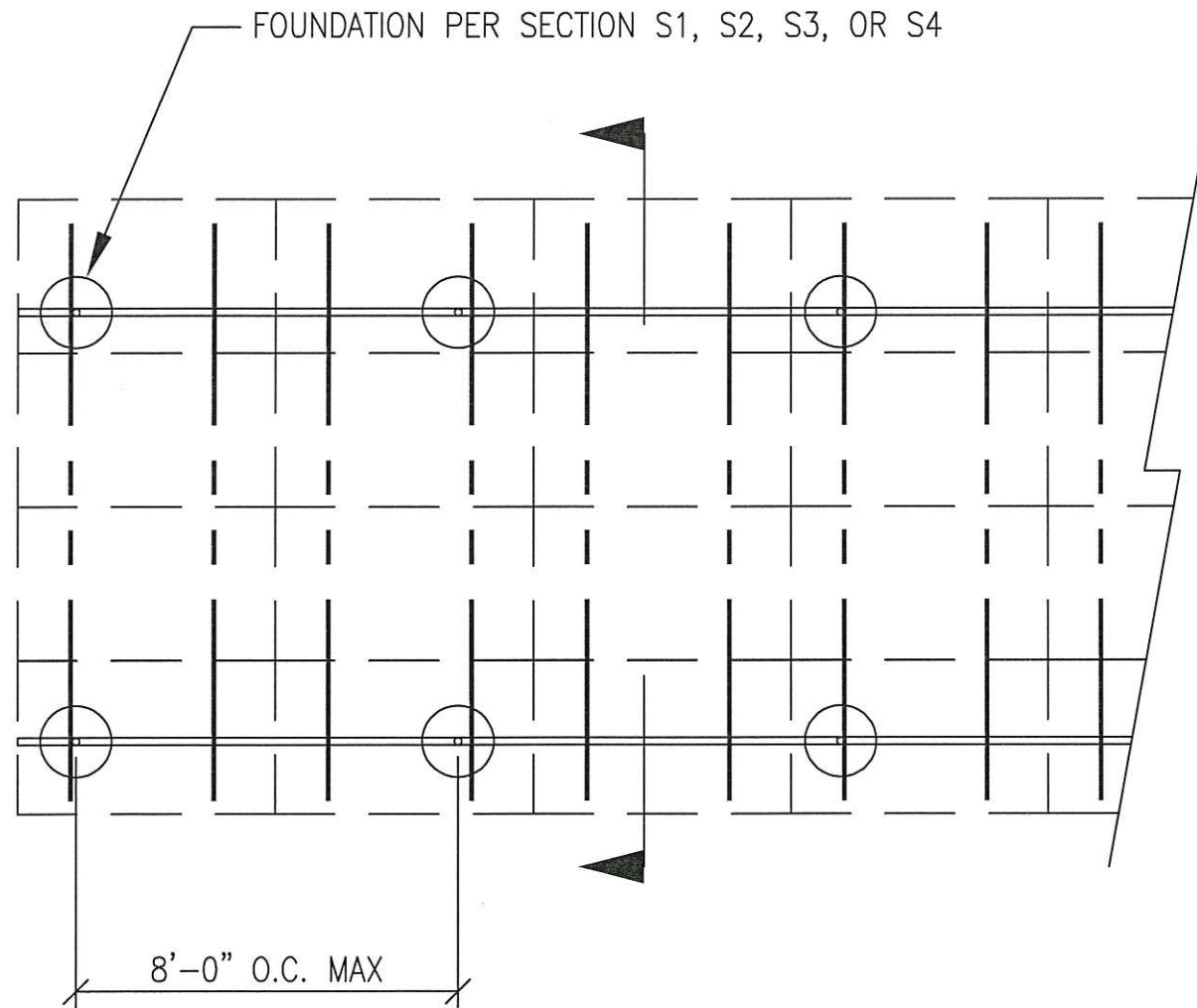


02/15/2019



JOB NO. U2716-072-181
 PROJECT BRITISH COLUMBIA GROUND MOUNTS
 SUBJECT ALL OPTIONS

651 W GALENA PARK BLVD. #101 (801) 990-1775
 DRAPER, UTAH 84020 (801) 990-1776 FAX



02/15/2019

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PV ARRAY PLAN

N.T.S.

P1



JOB NO. U2716-072-181

DATE 12/20/2018

PROJECT BRITISH COLUMBIA GROUND MOUNTS

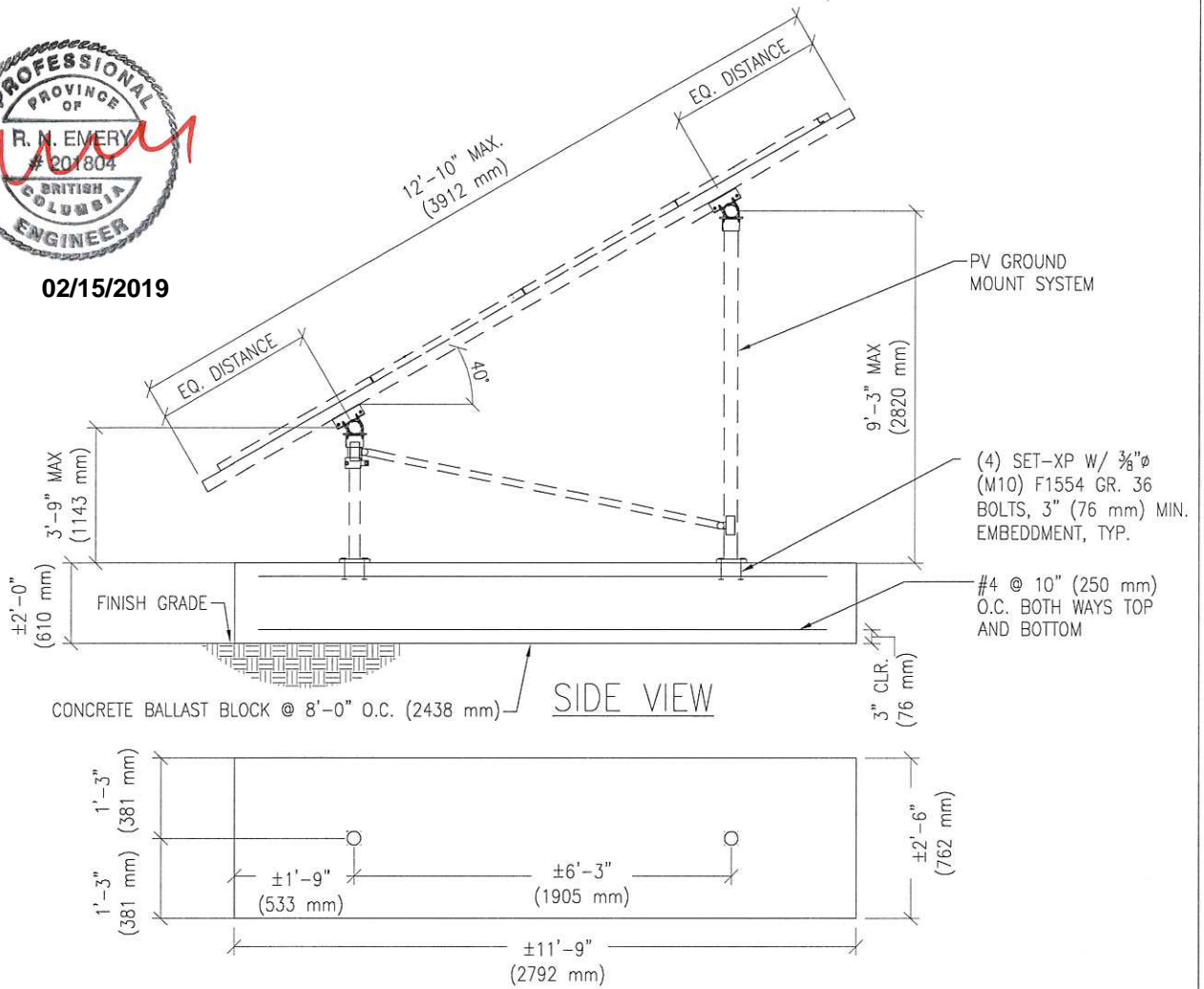
SUBJECT BALLASTED BLOCK OPTION DESIGNED STB CHECKED JSP

NOTES:

- For list of racking components see Sunmodo drawings dated 02/14/2019



02/15/2019



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PV ARRAY SECTION

N.T.S.

S4

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JOB NO. U2716-072-181

DATE 12/20/2018

PROJECT BRITISH COLUMBIA GROUND MOUNTS

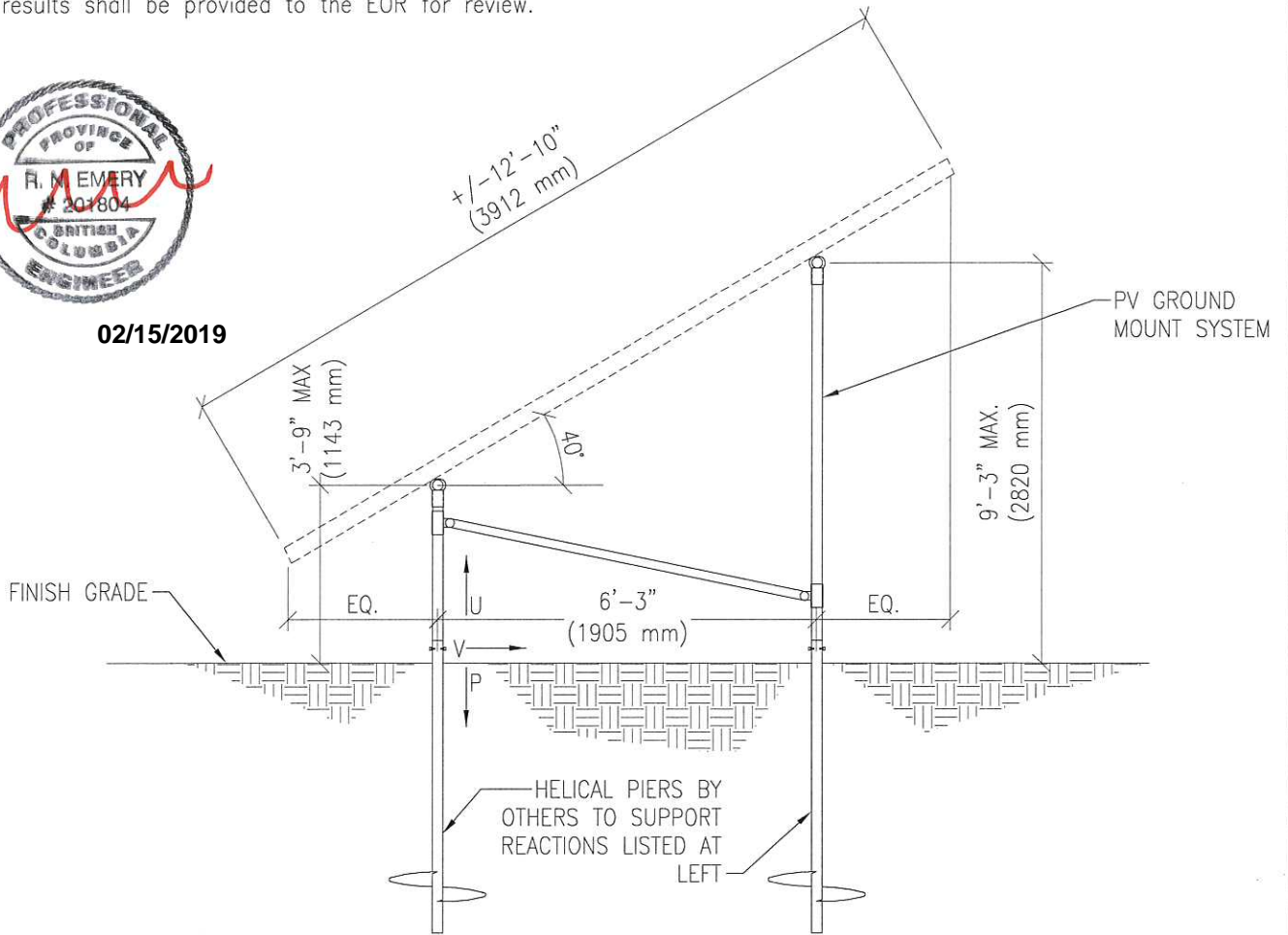
SUBJECT HELICAL PIER OPTION DESIGNED STB CHECKED JSP

NOTES:

1. For list of racking components see Sunmodo drawings dated 02/14/2019
2. Helical Piers shall be pull-tested per ASTM D3689
 - 2.1. Safety factor for uplift to be 1.5, S.F. for lateral loads to be 2.0
 - 2.2. Upward deflection limit = 1/2" (12.7 mm) Lateral deflection limit = 1" (25.4 mm)
 - 2.3. The load tests shall be performed by a certified testing company, and written results shall be provided to the EOR for review.



02/15/2019



MAXIMUM REACTIONS:	
U	= 2,400 LBS (10.67 kN)
P	= 2,900 LBS (12.90 kN)
V	= 1,900 LBS (8.45 kN)

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PV ARRAY SECTION

N.T.S.





JOB NO. U2716-072-181

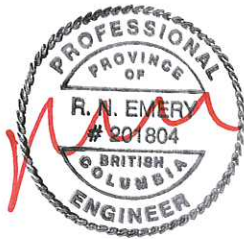
DATE 12/20/2018

PROJECT BRITISH COLUMBIA GROUND MOUNTS

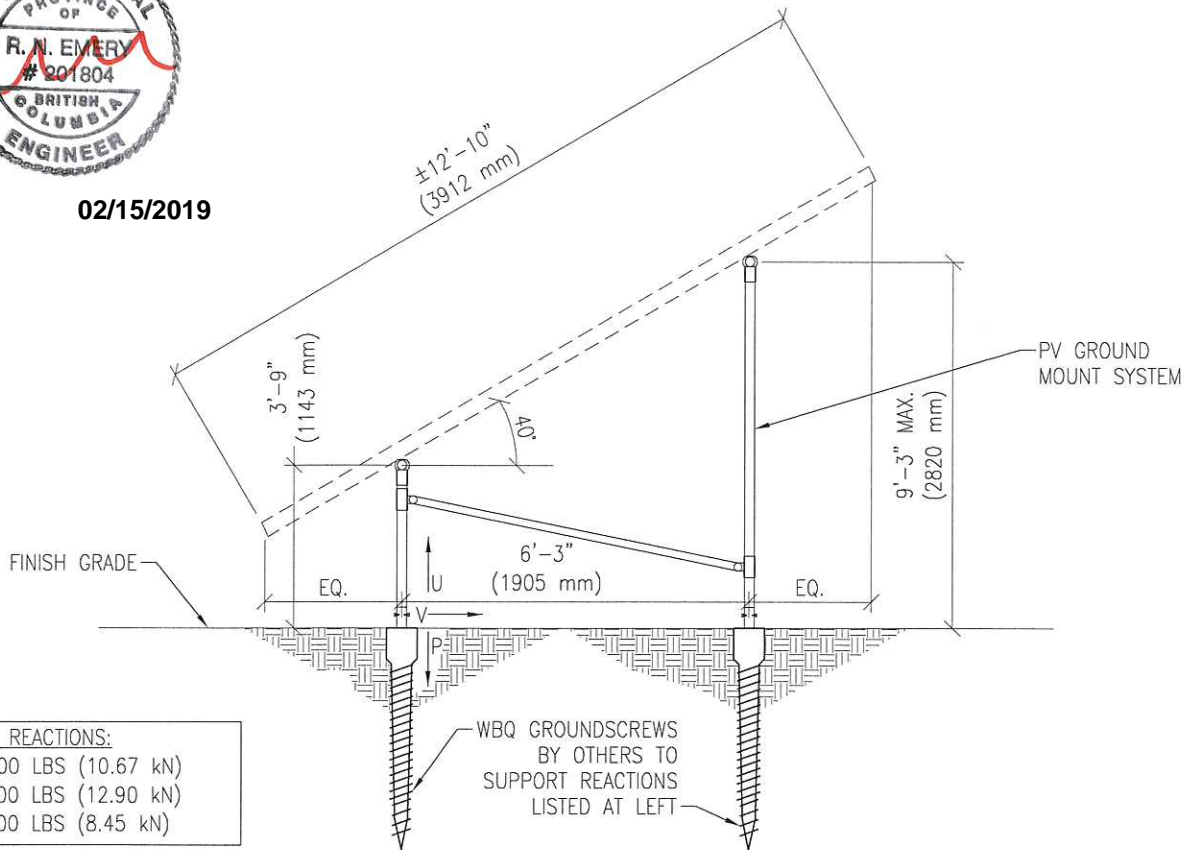
SUBJECT GROUND SCREW OPTION DESIGNED STB CHECKED JSP

NOTES:

1. For list of racking components see Sunmodo drawings dated 02/14/2019
2. Ground screws shall be pull-tested per ASTM D3689
 - 2.1. Safety factor for uplift to be 1.5, S.F. for lateral loads to be 2.0
 - 2.2. Upward deflection limit = 1/2" (12.7 mm) Lateral deflection limit = 1" (25.4 mm)
 - 2.3. The load tests shall be performed by a certified testing company, and written results shall be provided to the EOR for review.



02/15/2019



MAXIMUM REACTIONS:	
U	= 2,400 LBS (10.67 kN)
P	= 2,900 LBS (12.90 kN)
V	= 1,900 LBS (8.45 kN)

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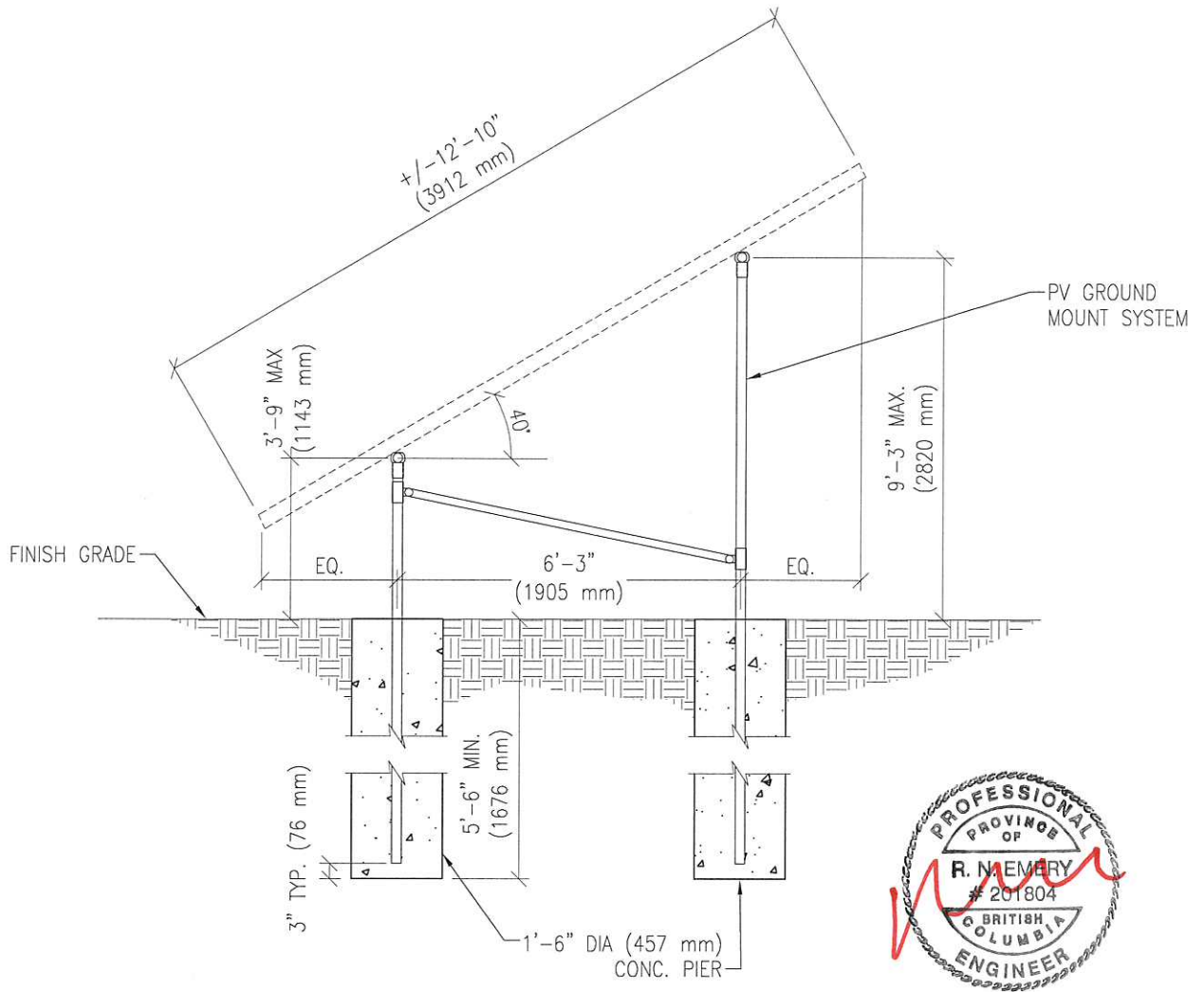
DATE 12/20/2018

PROJECT BRITISH COLUMBIA GROUND MOUNTS

SUBJECT DRILLED PIER OPTION DESIGNED STB CHECKED JSP

NOTES:

- For list of racking components see Sunmodo drawings dated 02/14/2019



02/15/2019

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PV ARRAY SECTION

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PROJECT: Ground Mount Package for British Columbia

SUBJECT: Dead Load

Design Weight:

		Metric	Unit
Individual Panel Weight [lb]:	50.7	23	kg
Panel Transverse Length (T5) [in]:	77.0	1956	mm
Panel Transverse Length (T5) [ft]:	6.4	1956	mm
Panel Longitudinal Length (L2) [in]:	39.1	993	mm
Panel Longitudinal Length (L2) [ft]:	3.3	993	mm
Individual Panel Area [ft ²]:	20.9	1.94	m ²
Individual Panel Weight [psf]:	2.4	0.12	kPa
# of Panels in Transverse Direction:	2		
Approximate Transverse Length (T4) [ft]:	12.8	3.91	m
# of Panels in Longitudinal Direction:	14		
Approximate Longitudinal Length (L1) [ft]:	45.6	13.90	m
Transverse Column Spacing (T1) [ft]:	6.5	1981	mm
Longitudinal Column Spacing (L3) [ft]:	8.0	2438	mm
# of Columns in Longitudinal Direction:	6		
# of Columns in Transverse Direction:	2		
Total Number of Columns:	12		
Panel Slope from Horizontal (a) [°]:	40.0		
Short Column Height (H1) [ft]:	3.8	1143	mm
Approximate Tall Column Height (H2) [ft]:	9.2	2805	mm
Transverse Brace between Columns :	Yes		
Approximate Brace Length (B1) [ft]:	8.0	2438	mm
Weight of Columns [plf]:	3.7	1.66	kg/ft
Weight of Cross Pipe [plf]:	3.7	1.7	kg/ft
Weight of Brace [plf]:	3.7	2	kg/ft
Tributary Transverse Length per Column [ft]:	6.4	1956	mm
Tributary Longitudinal Length per Column [ft]:	8.0	2438	mm
Tributary Area per Column [ft ²]:	51.3	4.8	m ²
Rail Weight [plf]:	1.0	0.5	kg/ft
Transverse Rail Weight per Column [lb]:	38.5	17.5	kg
Longitudinal Rail Weight per Column [lb]:	29.2	13.3	kg
Tall Column Weight [lb]:	33.6	15.3	kg
Panel Weight per Column [lb]:	124.5	56.6	kg
Rail Weight per Column [lb]:	38.5	17.5	kg
Cross Pipe Weight per Column [lb]:	29.2	13.3	kg
Brace Weight per Column [lb]:	14.6	7	kg

Total Weight per Column (1.0 D) [lb]: 240.4

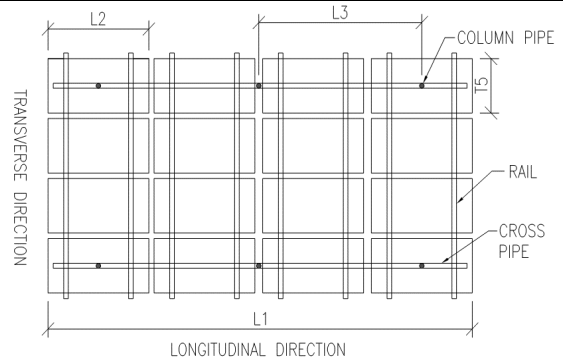


ILLUSTRATION ONLY

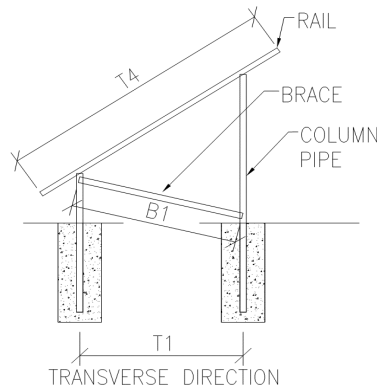


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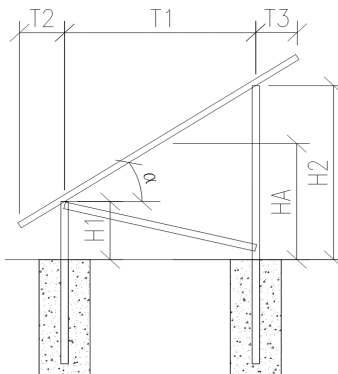


ILLUSTRATION ONLY

Assumptions:

- T2 = T3



JOB NO.: U2716-072-181

DESIGNED: STB

DATE: 02/14/19

PROJECT: Ground Mount Package for British Columbia

SUBJECT: Snow Load

SNOW LOAD (S):

			Metric	Unit
ASCE 7 Standard:	10	ASCE 7-10		
Panel Slope from Horizontal [°]:	40.0	Reference		
Snow Ground Load, p_g [psf]:	68.9	(Section 7.2)	3.3	kPa
Terrain Category:	C	(Table 7-2)		
Exposure of Roof:	Fully Exposed	(Table 7-2)		
Exposure Factor, C_e :	0.9	(Table 7-2)		
Thermal Factor, C_t :	1.2	(Table 7-3)		
Risk Category:	I	(Table 1.5-1)		
Importance Factor, I_s :	0.8	(Table 1.5-2)		
Flat Roof Snow Load, p_f [psf]:	42	(Equation 7.3-1)	2.0	kPa
Minimum Roof Snow Load, p_m [psf]:	0	(Section 7.3.4)	0	kPa
Unobstructed Slippery Surface?	Yes	(Section 7.4)		
Slope Factor Figure:	Figure 7-2c	(Section 7.4)		
Roof Slope Factor, C_s :	1.000	(Figure 7-2)		
Sloped Roof Snow Load, p_s [psf]:	42	(Equation 7.4-1)	2.0	kPa
Design Snow Load, S [psf]:	42		2.0	kPa
Tributary Transverse Length [ft]:	4.9		1498	mm
Tributary Longitudinal Length [ft]:	8		2438	mm
Tributary Area per Column [ft ²]:	39.3		3.7	m ²
Snow Load per Column (1.0 S) [lb]:	1639.2		7.29	kN



JOB NO.: U2716-072-181

DESIGNED: STB

DATE: 02/14/19

PROJECT: Ground Mount Package for British Columbia

SUBJECT: Wind Pressure

Design Wind Load:

ASCE 7 Standard:	10	ASCE 7-10
Basic Wind Speed, V [mph]:	105	Reference
Risk Category:	I	
Exposure Category	C	(Section 26.7.3)
Velocity Pressure Exposure Coefficient, K_h :	0.85	(Table 27.3-1)
Topographic Factor, K_{ht} :	1.0	(Section 26.8.2)
Wind Directionality Factor, K_d :	0.85	(Table 26.6-1)
Internal Pressure Coefficient, GC_{pi} :	0.00	(Table 26.11-1)
Velocity Pressure, q_h [psf]:	20.4	(Equation 27.3-1)
Gust Effect Factor, G:	0.85	(Section 26.9.1)
Panel Slope [degrees]:	40.0	

Metric	Unit
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46.9392 m/s

0.98 kPa

Net Pressure Coefficients (C_N) per: (Figure 27.4-4)

Clear Wind Flow	C_{NW}	C_{NL}
Case 1 ($\gamma = 0^\circ$, Load Case A)	-1.73	-1.80
Case 2 ($\gamma = 0^\circ$, Load Case B)	-2.37	-0.63
Case 3 ($\gamma = 180^\circ$, Load Case A)	2.13	2.30
Case 4 ($\gamma = 180^\circ$, Load Case B)	2.67	1.20

Design Wind Pressures (p) [psf] per: (Equation 27.4-3)

Clear Wind Flow	$q_h GC_{NW}$	$q_h GC_{NL}$
Case 1 ($\gamma = 0^\circ$, Load Case A)	-30.0	-31.2
Case 2 ($\gamma = 0^\circ$, Load Case B)	-41.0	-11.0
Case 3 ($\gamma = 180^\circ$, Load Case A)	37.0	39.9
Case 4 ($\gamma = 180^\circ$, Load Case B)	46.2	20.8

$q_h GC_{NW}$	$q_h GC_{NL}$	
-1.44	-1.49	kPa
-1.96	-0.53	kPa
1.77	1.91	kPa
2.21	1.00	kPa

Wind Pressure on Each Side of Panels [psf]

Clear Wind Flow	Short Col. Pressure	Long Col. Pressure
Case 1 ($\gamma = 0^\circ$, Load Case A)	-31.2	-30.0
Case 2 ($\gamma = 0^\circ$, Load Case B)	-11.0	-41.0
Case 3 ($\gamma = 180^\circ$, Load Case A)	37.0	39.9
Case 4 ($\gamma = 180^\circ$, Load Case B)	46.2	20.8

Short Col. Pressure	Long Col. Pressure	
-1.49	-1.44	kPa
-0.53	-1.96	kPa
1.77	1.91	kPa
2.21	1.00	kPa



JOB NO.: U2716-070-181

DESIGNED: STB

PROJECT: Ground Mount Package for Ontario Canada

Foundation Option 1: Drilled Concrete Pier



JOB NO.: U2716-072-181
DATE: 02/14/19

DESIGNED: STB

PROJECT: Ground Mount Package for British Columbia

Drilled Pier Design

Design Loads:

		Metric	Units			Metric	Units
Max. Shear, V [k]:	1.9	8.6	kN	Max. Down, P _d [k]:	3.9	17.3	kN
Max. Moment, M [k-ft]:	0.1	0.1	kN-m	Max. Uplift, P _u [k]:	2.5	11.1	kN

Pier Properties:

Pier Diameter, b [ft]:	1.5	457.2	mm	Volume of Concrete [ft ³]:	10	0.28	m ³
Min. Pier Diameter, b _{min} (opt'l) [ft]:				Volume of Concrete [yd ³]:	0.4	0.28	m ³
Top of Pier Elevation [ft]:	0.00	0	mm	Weight of Concrete [k]:	1.5	663	kg
Pier Depth, d [ft]:	5.5	1676.4	mm				
Min. Pier Depth, d _{min} (opt'l) [ft]:							
Max. Pier Depth, d _{max} (opt'l) [ft]:							

Soil Properties:

Allow. Bearing Pressure [psf]:	1,500	71.8	kPa	<u>Optional Parameters for Uplift:</u>			
1/3 increase for short term loads?	No			Skin Friction [psf]:	250	12.0	kPa
Lateral Bearing, S [pcf]:	150	23563	kN/m ³	Top Length to Ignore [ft]:	0.0	0	mm
Max. Lateral Bearing (opt'l) [psf]:				1/3 increase for short term loads?	No		
Top Depth to Ignore [ft]:	0.0			Combine w/ Bearing:	No		
1/3 increase for short term loads?	No						
1/2" deflection at t/o pier allowed:	Yes						

Check Bearing:

Bearing Capacity [k]:	6.5	28.8	kN	Bearing capacity OK.
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Check Uplift:

Uplift Capacity [k]:	7.8	34.7	kN	Uplift capacity OK.
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Check Lateral Bearing:

Applied Lateral Force, P [lb]:	1,930	8585	kN	
Point of Application, h [ft]:	0.1	16	mm	
S _{1_max} [psf]:			kPa	
S ₁ [psf]:	550	26.3	kPa	
A = 2.34*P/(S ₁ b):	5.47			
Required Pier Depth, d _{reqd} [ft]:	5.5	1676	mm	Lateral bearing capacity OK.

Foundation Option 2: Helical Pier

The helical piers must be tested to 1.5 times uplift and 2.0 times lateral reactions found in the table below.

Load (ASD)	Value (lbs / kN)	Factor of Safety	Test Value (lbs / kN)
UPLIFT	2400 / 10.7	1.5	3600 / 16.0
LATERAL	1900 / 8.5	2	3800 / 16.9

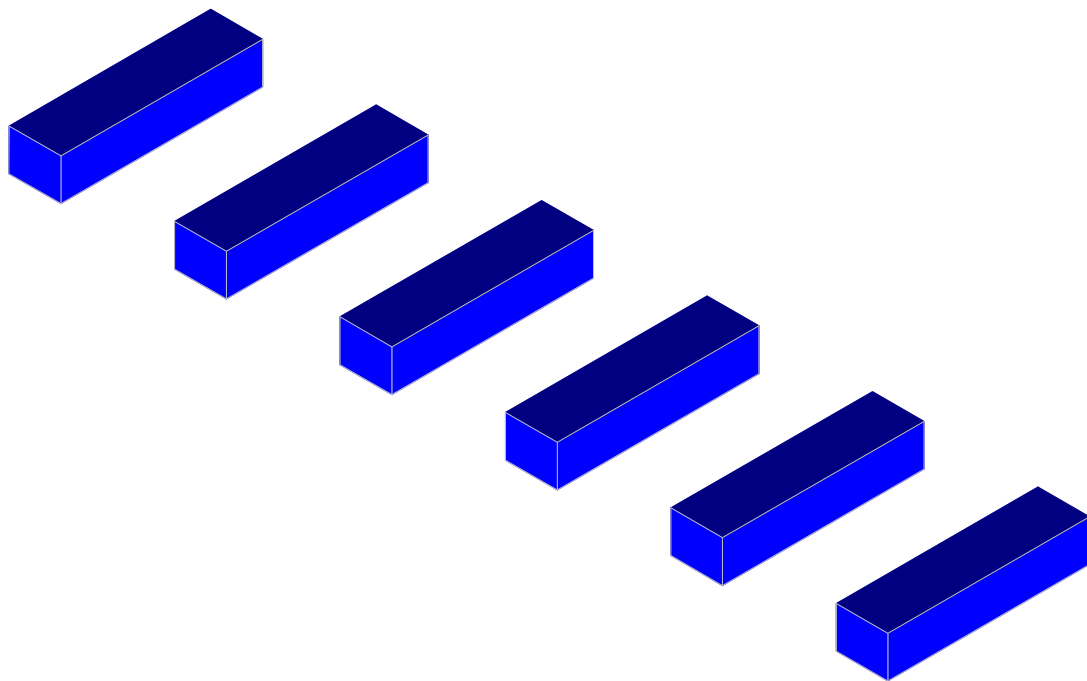


JOB NO.: U2716-070-181

DESIGNED: STB

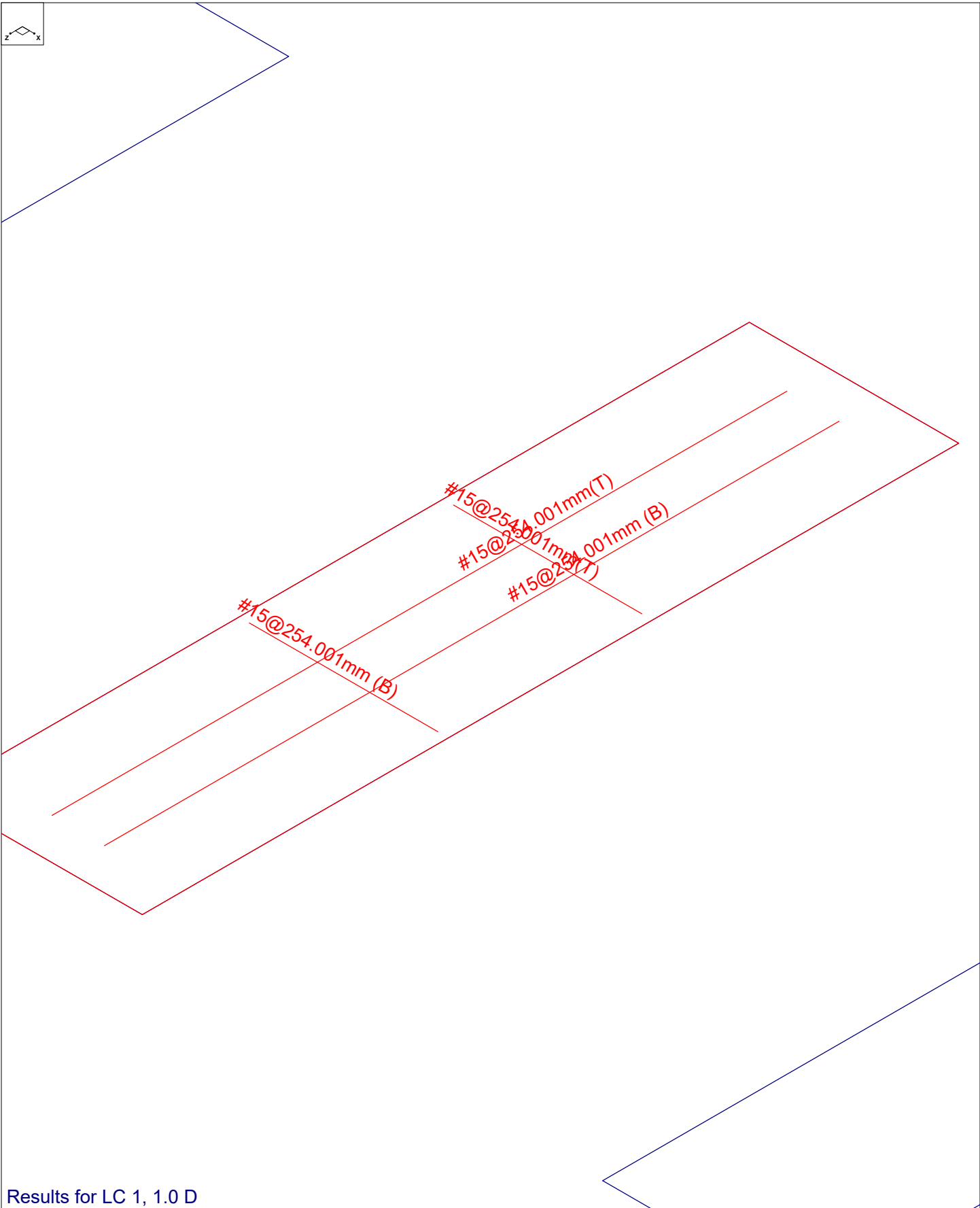
PROJECT: Ground Mount Package for Ontario Canada

Foundation Option 3: Ballasted Blocks



Results for LC 1, 1.0 D

Vector Structural Engineeri..	Ontario Ground Mount	SK - 19
STB		Feb 14, 2019 at 12:16 PM
U2716.070.181		BC GM 40 deg (2-12-19).r3d



Results for LC 1, 1.0 D

Vector Structural Engineeri...	Ontario Ground Mount	SK - 18
STB		Feb 14, 2019 at 12:15 PM
U2716.070.181		BC GM 40 deg (2-12-19).r3d

(Global) Model Settings

Display Sections for Member Calcs	5
Max Internal Sections for Member Calcs	100
Mesh Size (mm)	304.801
Max Iterations	10
Merge Tolerance (mm)	3.048
Solver	Sparse Accelerated
Coefficient of Friction	.25
No. of Shear Regions	4
Shear Region Spacing Increment (mm)	101.6
Min 1 Bar Dia Spacing for Beams?	No
Optimize footings for OTM / Sliding?	Yes
Parme Beta Factor	.65
Pile Safety Factor	3
Concrete Stress Block	Rectangular
Concrete Rebar Set	CSA G30.18
Concrete Code	CSA A23.3-14
HR Steel Pile Code	CSA S16-14
Wood Pile Code	AWC NDS-15: ASD

Concrete Properties

	Label	E [MPa]	G [MPa]	Nu	Therm (\...	Density[mt/m^3]	f _c [kPa]	Lambda	Flex Stee...	Shear St...
1	Conc3000NW	21759.674	9459.529	.15	.6	2.323	20684.101	1	4.137e+5	4.137e+5
2	Conc3500NW	23504.034	10217.946	.15	.6	2.323	24131.451	1	4.137e+5	4.137e+5
3	Conc4000NW	25124.288	10921.205	.15	.6	2.323	27578.801	1	4.137e+5	4.137e+5
4	Conc3000LW	14375.45	6253.493	.15	.6	1.762	20684.101	.75	4.137e+5	4.137e+5
5	Conc3500LW	15526.865	6749.912	.15	.6	1.762	24131.451	.75	4.137e+5	4.137e+5
6	Conc4000LW	16602.438	7218.751	.15	.6	1.762	27578.801	.75	4.137e+5	4.137e+5

Slab Rebar Parameters

	Label	Top Bar	Bottom Bar	Max Top Bar Sp...	Min Top Bar Sp...	Max Bot Bar Sp...	Min Bot Bar Sp...	Spacing Incr...	Rebar Options
1	Typical	#15	#15	254.001	254.001	254.001	254.001	25.4	Optimize

Soil Definitions

	Label	Subgrade Modulus[mt/m^3]	Allowable Bearing[kPa]	Depth Properties	Default?
1	Default	1601.84	71.82	None	Yes

Slabs

	Label	Thickness [mm]	Material	Local Axis Angle [deg]	Analysis Offset [mm]
1	S1	609.601	Conc3000NW	0	0
2	S2	609.601	Conc3000NW	0	0
3	S3	609.601	Conc3000NW	0	0
4	S4	609.601	Conc3000NW	0	0
5	S5	609.601	Conc3000NW	0	0
6	S6	609.601	Conc3000NW	0	0

Load Combinations

	Label	Solve	Service	A...	SF	Cat...	Fa...	Cat...	Fa...	Cat...	Fa...	Cat...	Fa...	Cat...	Fa...	Cat...	Fa...	C...	Fa...	C...	Fa...	
1	1.0 D	Yes	Yes	1.5	DL	1																
2	1.0 D ...	Yes	Yes	1.5	DL	1	RLL	1														
3	1.0 D ...	Yes	Yes	1.5	DL	1	RLL		OL1	.6												
4	1.0 D ...	Yes	Yes	1.5	DL	1	RLL		OL2	.6												
5	1.0 D ...	Yes	Yes	1.5	DL	1	RLL		OL3	.6												

Load Combinations (Continued)

Label	Solve	Service A	SF	Cat	Fa	Cat	Fa	Cat	Fa	Cat	Fa	Cat	Fa	Cat	Fa	Cat	Fa	Cat	Fa
6	1.0 D ...	Yes	Yes	1.5	DL	1	RLL		OL4	.6									
7	1.0 D ...	Yes	Yes	1.5	DL	1	RLL		OL5	.6									
8	1.0 D ...	Yes	Yes	1.5	DL	1	RLL		OL6	.6									
9	1.0 D ...	Yes	Yes	1.5	DL	1	RLL	.75	OL1	.45									
10	1.0 D ...	Yes	Yes	1.5	DL	1	RLL	.75	OL2	.45									
11	1.0 D ...	Yes	Yes	1.5	DL	1	RLL	.75	OL3	.45									
12	1.0 D ...	Yes	Yes	1.5	DL	1	RLL	.75	OL4	.45									
13	1.0 D ...	Yes	Yes	1.5	DL	1	RLL	.75	OL5	.45									
14	1.0 D ...	Yes	Yes	1.5	DL	1	RLL	.75	OL6	.45									
15	0.6 D ...	Yes	Yes	1.1	DL	.6	RLL		OL1	.6									
16	0.6 D ...	Yes	Yes	1.1	DL	.6	RLL		OL2	.6									
17	0.6 D ...	Yes	Yes	1.1	DL	.6	RLL		OL3	.6									
18	0.6 D ...	Yes	Yes	1.1	DL	.6	RLL		OL4	.6									
19	0.6 D ...	Yes	Yes	1.1	DL	.6	RLL		OL5	.6									
20	0.6 D ...	Yes	Yes	1.1	DL	.6	RLL		OL6	.6									
21																			
22	1.4D	Yes			DL	1.4													
23	1.2D+...	Yes			DL	1.2	SL	1.6											
24	1.2D+...	Yes			DL	1.2	SL	1.6	OL1	.5									
25	1.2D+...	Yes			DL	1.2	SL	1.6	OL2	.5									
26	1.2D+...	Yes			DL	1.2	SL	1.6	OL3	.5									
27	1.2D+...	Yes			DL	1.2	SL	1.6	OL4	.5									
28	1.2D+...	Yes			DL	1.2	SL	1.6	OL5	.5									
29	1.2D+...	Yes			DL	1.2	SL	1.6	OL6	.5									
30	1.2D+...	Yes			DL	1.2			OL1	1									
31	1.2D-1...	Yes			DL	1.2			OL2	1									
32	1.2D+...	Yes			DL	1.2			OL3	1									
33	1.2D-1...	Yes			DL	1.2			OL4	1									
34	1.2D+...	Yes			DL	1.2			OL5	1									
35	1.2D-1...	Yes			DL	1.2			OL6	1									
36	.9D+1....	Yes			DL	.9			OL1	1									
37	.9D-1....	Yes			DL	.9			OL2	1									
38	.9D+1....	Yes			DL	.9			OL3	1									
39	.9D-1....	Yes			DL	.9			OL4	1									
40	.9D+1....	Yes			DL	.9			OL5	1									
41	.9D-1....	Yes			DL	.9			OL6	1									

Design Strips

	Label	Rebar Angle from Pl...	No. of Design Cuts	Design Rule
1	DS1	0	50	Typical
2	DS2	90	50	Typical



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E-mail:			

1. Project information

Customer company:
Customer contact name:
Customer e-mail:
Comment:

Project description:
Location:
Fastening description:

2. Input Data & Anchor Parameters

General

Design method: ACI 318-05
Units: Imperial units

Anchor Information:

Anchor type: Bonded anchor
Material: F1554 Grade 36
Diameter (inch): 0.375
Effective Embedment depth, h_{ef} (inch): 3.000
Code report: ICC-ES ESR-2508
Anchor category: -
Anchor ductility: Yes
 h_{min} (inch): 4.88
 c_{ac} (inch): 3.62
 C_{min} (inch): 1.75
 S_{min} (inch): 3.00

Base Material

Concrete: Normal-weight
Concrete thickness, h (inch): 34.00
State: Cracked
Compressive strength, f'_c (psi): 2500
 $\Psi_{c,v}$: 1.0
Reinforcement condition: B tension, B shear
Supplemental reinforcement: Not applicable
Reinforcement provided at corners: No
Ignore concrete breakout in tension: No
Ignore concrete breakout in shear: No
Hole condition: Dry concrete
Inspection: Continuous
Temperature range, Short/Long: 150/110°F
Ignore 6do requirement: Not applicable
Build-up grout pad: No

Base Plate

Length x Width x Thickness (inch): 4.75 x 4.75 x 0.31
Yield stress: 34084 psi

Profile type/size: Pipe1-1/2STD

Recommended Anchor

Anchor Name: SET-XP® - SET-XP w/ 3/8"Ø F1554 Gr. 36
Code Report: ICC-ES ESR-2508





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Load and Geometry

Load factor source: ACI 318 Section 9.2

Load combination: not set

Seismic design: No

Anchors subjected to sustained tension: No

Apply entire shear load at front row: No

Anchors only resisting wind and/or seismic loads: No

Strength level loads:

N_{ua} [lb]: 2400

V_{uax} [lb]: 127

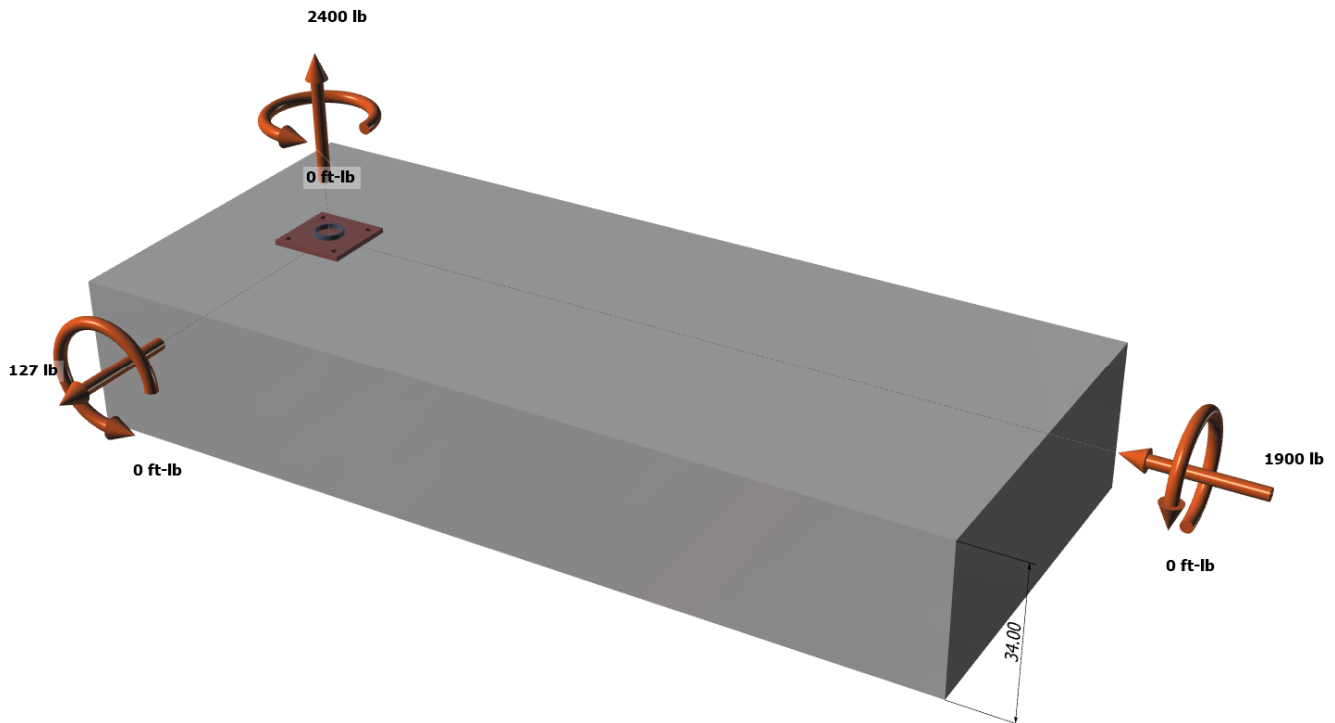
V_{uay} [lb]: -1900

M_{ux} [ft-lb]: 0

M_{uy} [ft-lb]: 0

M_{uz} [ft-lb]: 0

<Figure 1>





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<Figure 2>





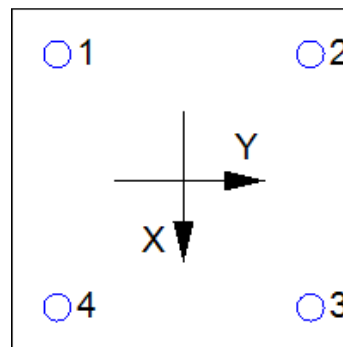
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3. Resulting Anchor Forces

Anchor	Tension load, N _{ua} (lb)	Shear load x, V _{uax} (lb)	Shear load y, V _{uay} (lb)	Shear load combined, $\sqrt{(V_{uax})^2 + (V_{uay})^2}$ (lb)
1	600.0	31.8	-475.0	476.1
2	600.0	31.8	-475.0	476.1
3	600.0	31.8	-475.0	476.1
4	600.0	31.8	-475.0	476.1
Sum	2400.0	127.0	-1900.0	1904.2

Maximum concrete compression strain (‰): 0.00
 Maximum concrete compression stress (psi): 0
 Resultant tension force (lb): 2400
 Resultant compression force (lb): 0
 Eccentricity of resultant tension forces in x-axis, e'_{Nx} (inch): 0.00
 Eccentricity of resultant tension forces in y-axis, e'_{Ny} (inch): 0.00
 Eccentricity of resultant shear forces in x-axis, e'_{Vx} (inch): 0.00
 Eccentricity of resultant shear forces in y-axis, e'_{Vy} (inch): 0.00

<Figure 3>



4. Steel Strength of Anchor in Tension (Sec. D.5.1)

N _{sa} (lb)	φ	φN _{sa} (lb)
4525	0.75	3394

5. Concrete Breakout Strength of Anchor in Tension (Sec. D.5.2)

$$N_b = k_c \lambda \sqrt{f_c} h_{ef}^{1.5} \text{ (Eq. D-7)}$$

k _c	λ	f _c (psi)	h _{ef} (in)	N _b (lb)
17.0	1.00	2500	3.000	4417

$$\phi N_{cbg} = \phi (A_{Nc} / A_{Nco}) \psi_{ec,N} \psi_{ed,N} \psi_{c,N} \psi_{cp,N} N_b \text{ (Sec. D.4.1 \& Eq. D-5)}$$

A _{Nc} (in ²)	A _{Nco} (in ²)	c _{a,min} (in)	ψ _{ec,N}	ψ _{ed,N}	ψ _{c,N}	ψ _{cp,N}	N _b (lb)	φ	φN _{cbg} (lb)
156.25	81.00	7.25	1.000	1.000	1.00	1.000	4417	0.65	5538

6. Adhesive Strength of Anchor in Tension (AC308 Sec. 3.3)

$$\tau_{k,cr} = \tau_{k,cr} f_{short-term} K_{sat}$$

τ _{k,cr} (psi)	f _{short-term}	K _{sat}	τ _{k,cr} (psi)
595	1.00	1.00	595

$$N_{a0} = \tau_{k,cr} \pi d_a h_{ef} \text{ (Eq. D-16f)}$$

τ _{k,cr} (psi)	d _a (in)	h _{ef} (in)	N _{a0} (lb)
595	0.38	3.000	2103

$$\phi N_{ag} = \phi (A_{Na} / A_{Na0}) \psi_{ed,Na} \psi_{g,Na} \psi_{ec,Na} \psi_{p,Na} N_{a0} \text{ (Sec. D.4.1 \& Eq. D-16b)}$$

A _{Na} (in ²)	A _{Na0} (in ²)	ψ _{ed,Na}	ψ _{g,Na}	ψ _{ec,Na}	ψ _{p,Na}	N _{a0} (lb)	φ	φN _{ag} (lb)
80.38	29.87	1.000	1.134	1.000	1.000	2103	0.65	4171



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8. Steel Strength of Anchor in Shear (Sec. D.6.1)

V_{sa} (lb)	ϕ_{grout}	ϕ	$\phi_{grout}\phi V_{sa}$ (lb)
2260	1.0	0.65	1469

9. Concrete Breakout Strength of Anchor in Shear (Sec. D.6.2)

Shear perpendicular to edge in x-direction:

$$V_{bx} = 7(l_e / d_a)^{0.2} \sqrt{d_a \lambda} \sqrt{f_c c_{a1}^{1.5}} \text{ (Eq. D-24)}$$

l_e (in)	d_a (in)	λ	f_c (psi)	c_{a1} (in)	V_{bx} (lb)
3.00	0.375	1.00	2500	13.75	16564

$$\phi V_{cbgx} = \phi (A_{Vc} / A_{Vco}) \psi_{ec,v} \psi_{ed,v} \psi_{c,v} \psi_{h,v} V_{bx} \text{ (Sec. D.4.1 \& Eq. D-22)}$$

A_{Vc} (in ²)	A_{Vco} (in ²)	$\psi_{ec,v}$	$\psi_{ed,v}$	$\psi_{c,v}$	$\psi_{h,v}$	V_{bx} (lb)	ϕ	ϕV_{cbgx} (lb)
647.11	850.78	1.000	0.805	1.000	1.000	16564	0.70	7103

Shear perpendicular to edge in y-direction:

$$V_{by} = 7(l_e / d_a)^{0.2} \sqrt{d_a \lambda} \sqrt{f_c c_{a1}^{1.5}} \text{ (Eq. D-24)}$$

l_e (in)	d_a (in)	λ	f_c (psi)	c_{a1} (in)	V_{by} (lb)
3.00	0.375	1.00	2500	10.75	11450

$$\phi V_{cbgy} = \phi (A_{Vc} / A_{Vco}) \psi_{ec,v} \psi_{ed,v} \psi_{c,v} \psi_{h,v} V_{by} \text{ (Sec. D.4.1 \& Eq. D-22)}$$

A_{Vc} (in ²)	A_{Vco} (in ²)	$\psi_{ec,v}$	$\psi_{ed,v}$	$\psi_{c,v}$	$\psi_{h,v}$	V_{by} (lb)	ϕ	ϕV_{cbgy} (lb)
387.00	520.03	1.000	0.891	1.000	1.000	11450	0.70	5313

Shear parallel to edge in x-direction:

$$V_{by} = 7(l_e / d_a)^{0.2} \sqrt{d_a \lambda} \sqrt{f_c c_{a1}^{1.5}} \text{ (Eq. D-24)}$$

l_e (in)	d_a (in)	λ	f_c (psi)	c_{a1} (in)	V_{by} (lb)
3.00	0.375	1.00	2500	7.25	6342

$$\phi V_{cbgx} = \phi (2)(A_{Vc} / A_{Vco}) \psi_{ec,v} \psi_{ed,v} \psi_{c,v} \psi_{h,v} V_{by} \text{ (Sec. D.4.1, D.6.2.1(c) \& Eq. D-22)}$$

A_{Vc} (in ²)	A_{Vco} (in ²)	$\psi_{ec,v}$	$\psi_{ed,v}$	$\psi_{c,v}$	$\psi_{h,v}$	V_{by} (lb)	ϕ	ϕV_{cbgx} (lb)
261.00	236.53	1.000	1.000	1.000	1.000	6342	0.70	9797

Shear parallel to edge in y-direction:

$$V_{bx} = 7(l_e / d_a)^{0.2} \sqrt{d_a \lambda} \sqrt{f_c c_{a1}^{1.5}} \text{ (Eq. D-24)}$$

l_e (in)	d_a (in)	λ	f_c (psi)	c_{a1} (in)	V_{bx} (lb)
3.00	0.375	1.00	2500	10.25	10661

$$\phi V_{cbgy} = \phi (2)(A_{Vc} / A_{Vco}) \psi_{ec,v} \psi_{ed,v} \psi_{c,v} \psi_{h,v} V_{bx} \text{ (Sec. D.4.1, D.6.2.1(c) \& Eq. D-22)}$$

A_{Vc} (in ²)	A_{Vco} (in ²)	$\psi_{ec,v}$	$\psi_{ed,v}$	$\psi_{c,v}$	$\psi_{h,v}$	V_{bx} (lb)	ϕ	ϕV_{cbgy} (lb)
401.67	472.78	1.000	1.000	1.000	1.000	10661	0.70	12680

10. Concrete Pryout Strength of Anchor in Shear (Sec. D.6.3)

$$\phi V_{cp} = \phi \min[K_{cp} N_{ag}; K_{cp} N_{cbg}] = \phi \min[K_{cp}(A_{Na} / A_{Na0}) \psi_{ed,Na} \psi_{g,Na} \psi_{ec,Na} \psi_{p,Na} N_{a0}; K_{cp}(A_{Nc} / A_{Nco}) \psi_{ec,N} \psi_{ed,N} \psi_{c,N} \psi_{cp,N} N_b] \text{ (Eq. D-30b)}$$

K_{cp}	A_{Na} (in ²)	A_{Na0} (in ²)	$\psi_{ed,Na}$	$\psi_{g,Na}$	$\psi_{ec,Na}$	$\psi_{p,Na}$	N_{a0} (lb)	N_a (lb)
2.0	80.38	29.87	1.000	1.134	1.000	1.000	2103	6418

A_{Nc} (in ²)	A_{Nco} (in ²)	$\psi_{ec,N}$	$\psi_{ed,N}$	$\psi_{c,N}$	$\psi_{cp,N}$	N_b (lb)	N_{cb} (lb)	ϕ
156.25	81.00	1.000	1.000	1.000	1.000	4417	8520	0.70



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ϕV_{cpq} (lb)
8985

11. Results

Interaction of Tensile and Shear Forces (Sec. RD.7)

Tension	Factored Load, N_{ua} (lb)	Design Strength, ϕN_n (lb)	Ratio	Status	
Steel	600	3394	0.18	Pass	
Concrete breakout	2400	5538	0.43	Pass	
Adhesive	2400	4171	0.58	Pass (Governs)	
Shear	Factored Load, V_{ua} (lb)	Design Strength, ϕV_n (lb)	Ratio	Status	
Steel	476	1469	0.32	Pass	
T Concrete breakout x+	127	7103	0.02	Pass	
T Concrete breakout y-	1900	5313	0.36	Pass	
Concrete breakout y-	64	9797	0.01	Pass	
Concrete breakout x-	950	12680	0.07	Pass	
Concrete breakout, combined	-	-	0.36	Pass (Governs)	
Pryout	1904	8985	0.21	Pass	
Interaction check	$(N_{ua}/\phi N_{ua})^{5/3}$	$(V_{ua}/\phi V_{ua})^{5/3}$	Combined Ratio	Permissible	Status
Sec. RD.7	0.40	0.18	57.9%	1.0	Pass

SET-XP w/ 3/8"Ø F1554 Gr. 36 with hef = 3.000 inch meets the selected design criteria.

12. Warnings

- When cracked concrete is selected, concrete compressive strength used in concrete breakout strength in tension, adhesive strength in tension and concrete pryout strength in shear for SET-XP adhesive anchor is limited to 2,500 psi per ICC-ES ESR-2508 Section 5.3.
- Designer must exercise own judgement to determine if this design is suitable.
- Refer to manufacturer's product literature for hole cleaning and installation instructions.

Foundation Option 4: Ground Screws

The helical piers must be tested to 1.5 times uplift and 2.0 times lateral reactions found in the table below.

Capacity of ground screws is based of testing by BAYO.S in semi-solid clay. The ground screws must be tested to 1.5 times uplift and 2.0 times lateral reactions found in the table below.

Load (ASD)	Value (lbs / kN)	Factor of Safety	Test Value (lbs / kN)
UPLIFT	2400 / 10.7	1.5	3600 / 16.0
LATERAL	1900 / 8.5	2	3800 / 16.9

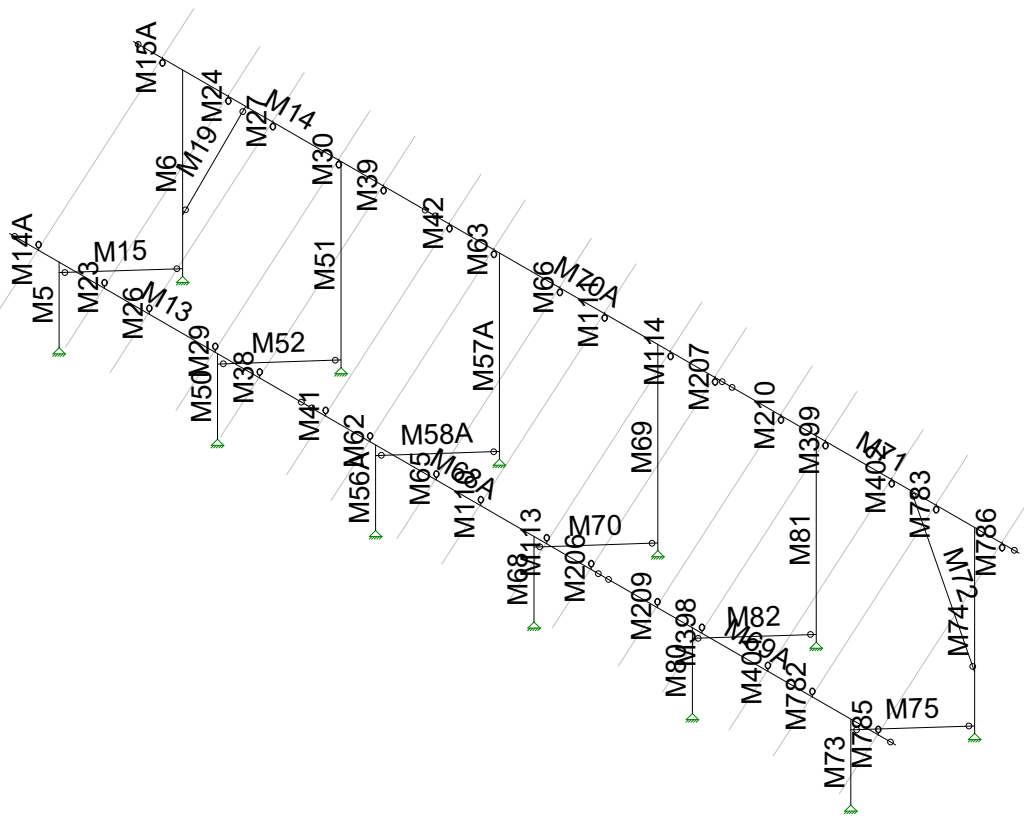


JOB NO.: U2716-070-181

DESIGNED: STB

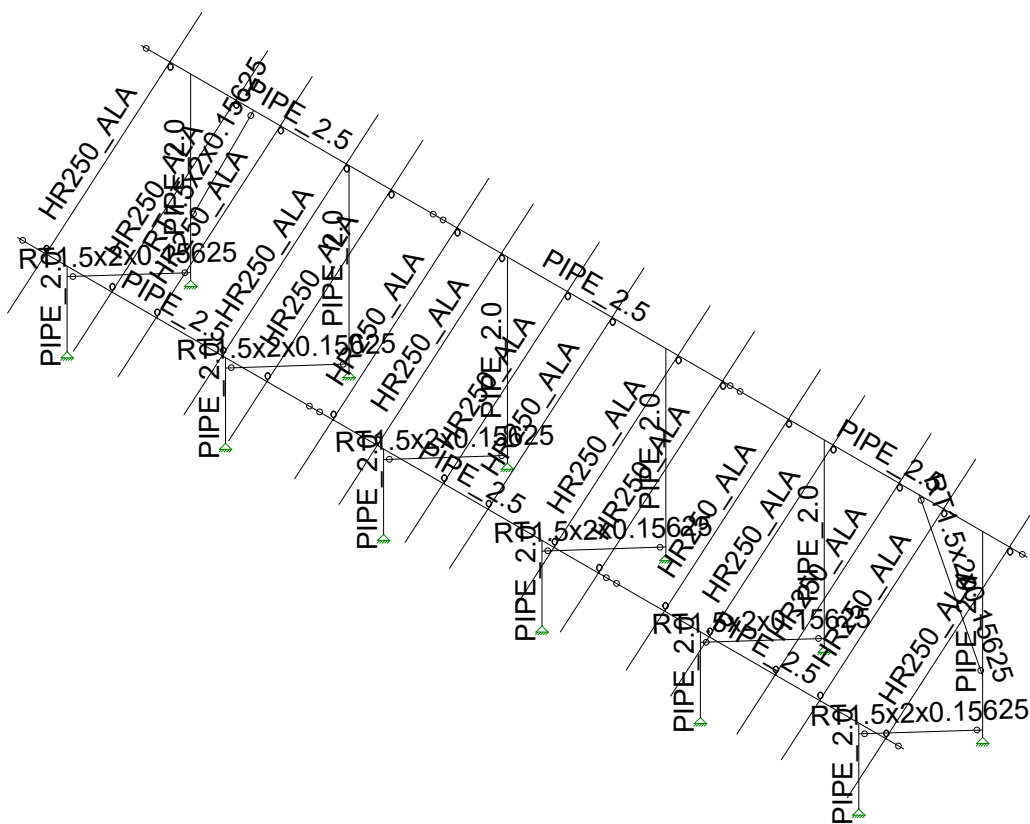
PROJECT: Ground Mount Package for Ontario Canada

Framing Analysis



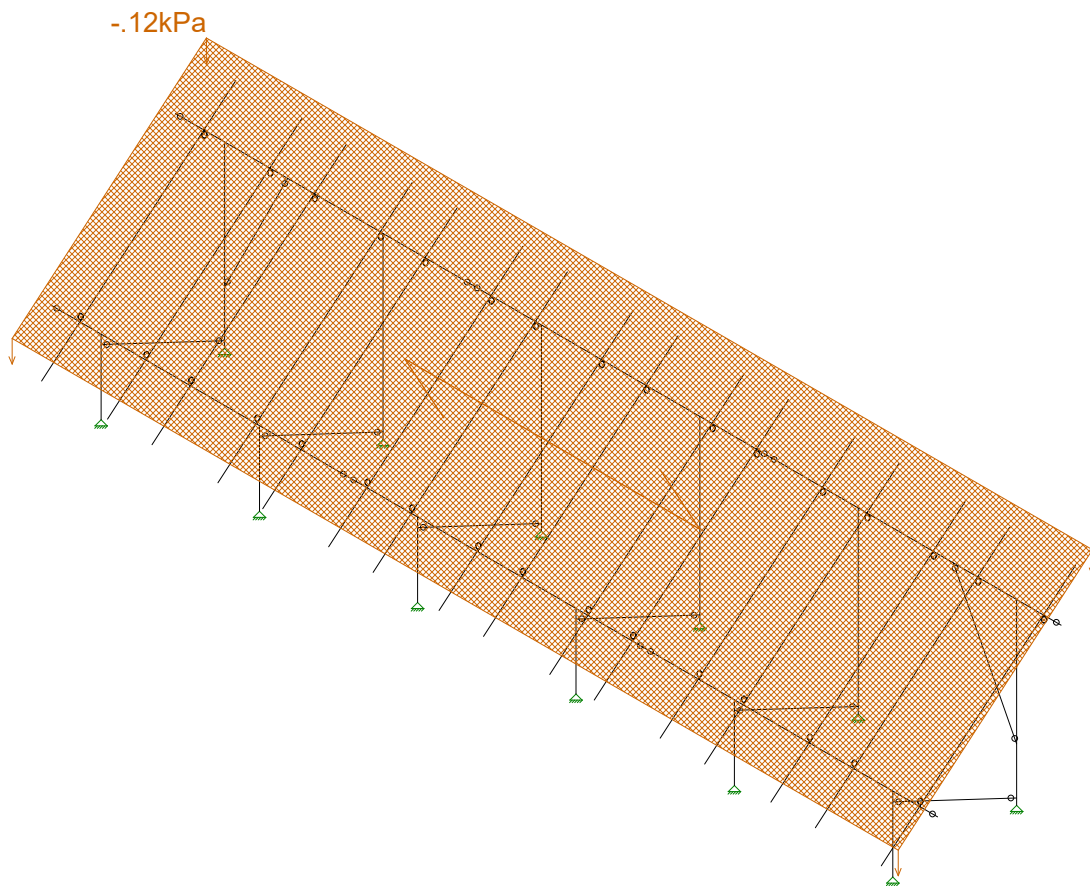
Envelope Only Solution

Vector Structural Engineeri...	BC Ground Mount	SK - 6
STB		Feb 14, 2019 at 12:11 PM
U2716.072.181		BC GM 40 deg (2-12-19).r3d



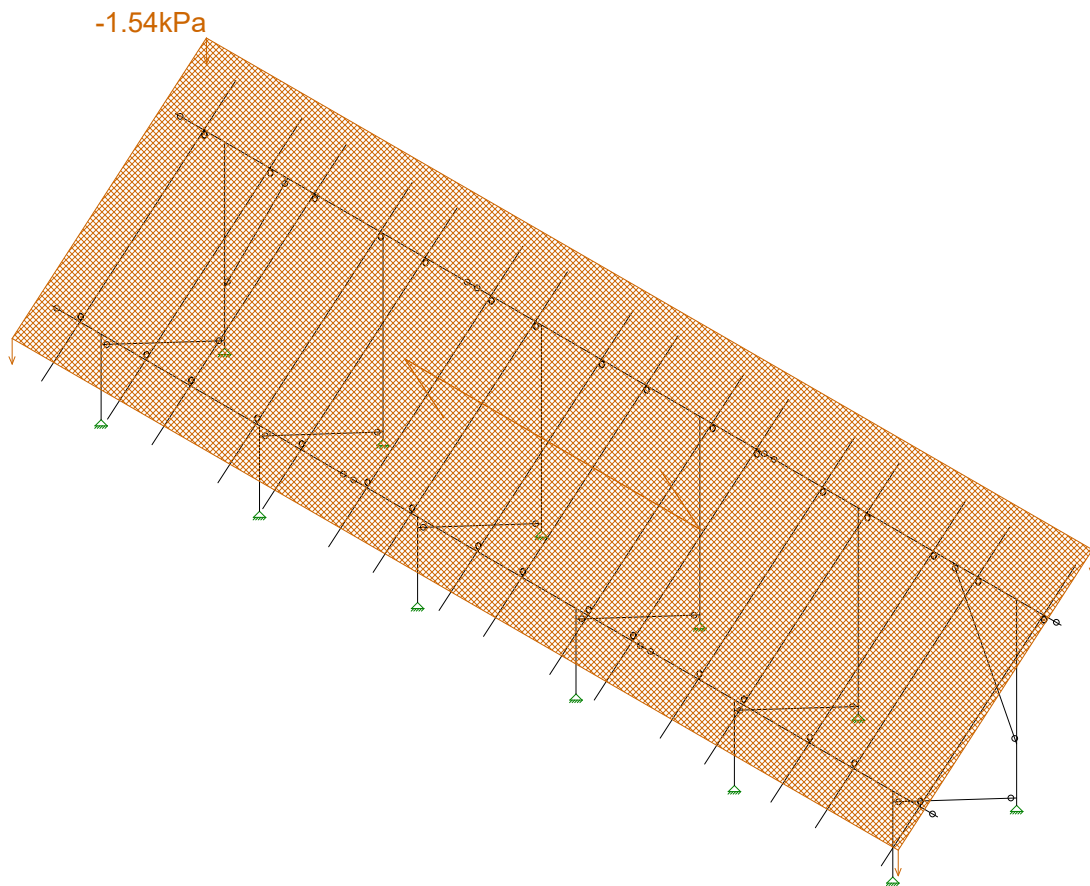
Envelope Only Solution

Vector Structural Engineeri...	BC Ground Mount	SK - 7
STB		Feb 14, 2019 at 12:11 PM
U2716.072.181		BC GM 40 deg (2-12-19).r3d



Loads: BLC 2, Solar Panel Weight
Envelope Only Solution

Vector Structural Engineeri..	BC Ground Mount	SK - 8
STB		Feb 14, 2019 at 12:11 PM
U2716.072.181		BC GM 40 deg (2-12-19).r3d



Loads: BLC 3, Roof Live/Snow
Envelope Only Solution

Vector Structural Engineeri..

STB

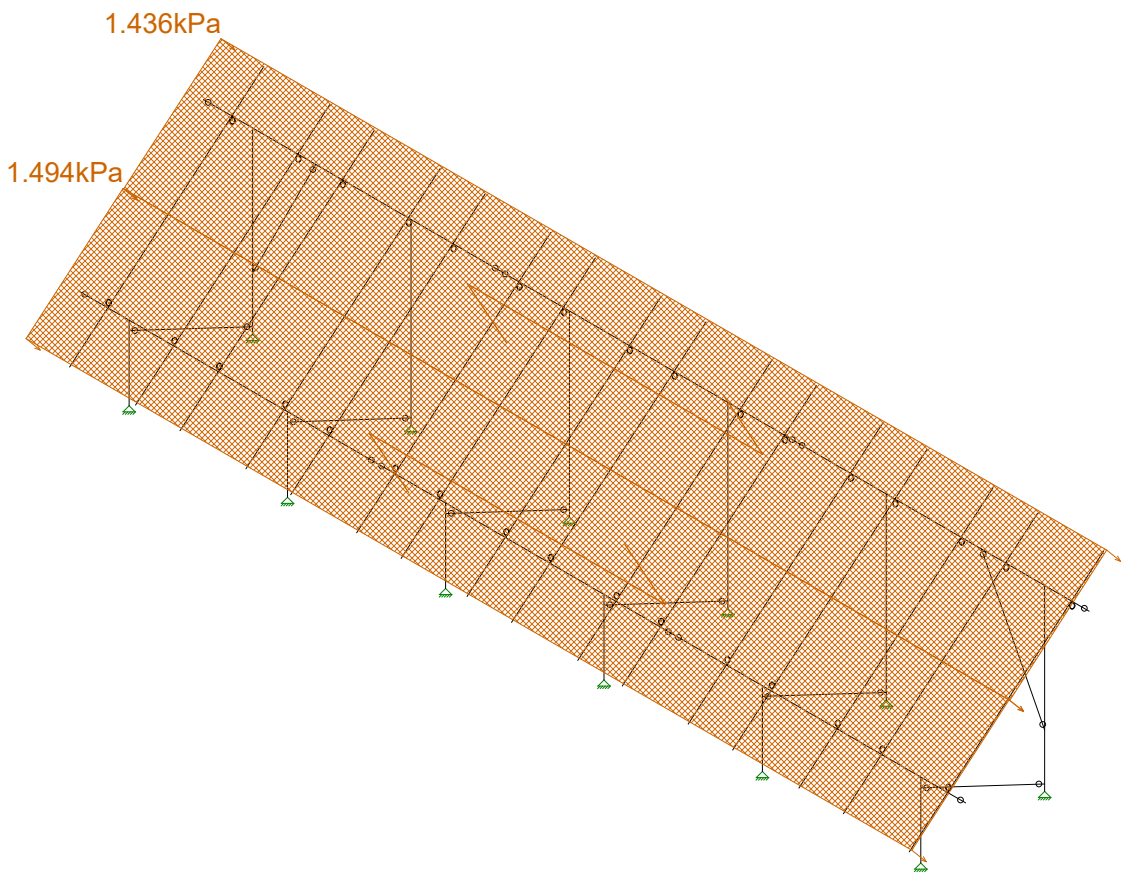
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BC Ground Mount

SK - 9

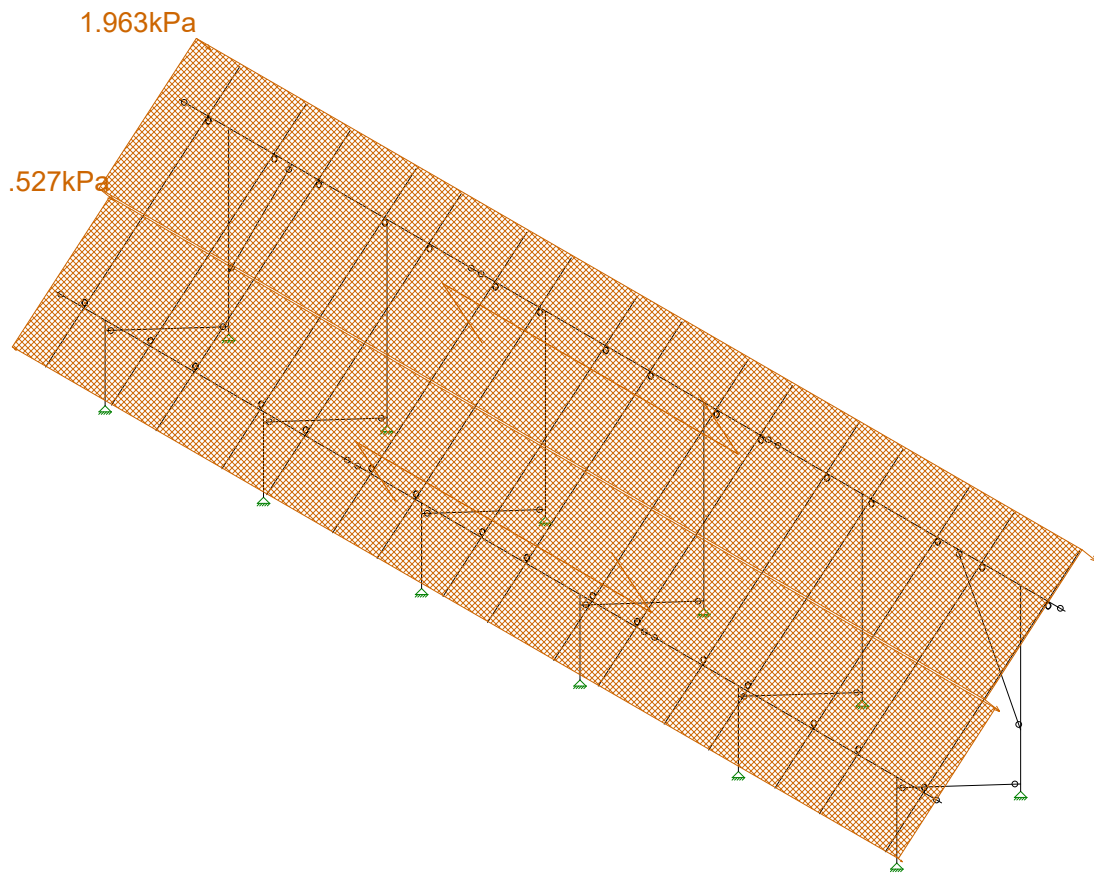
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BC GM 40 deg (2-12-19).r3d



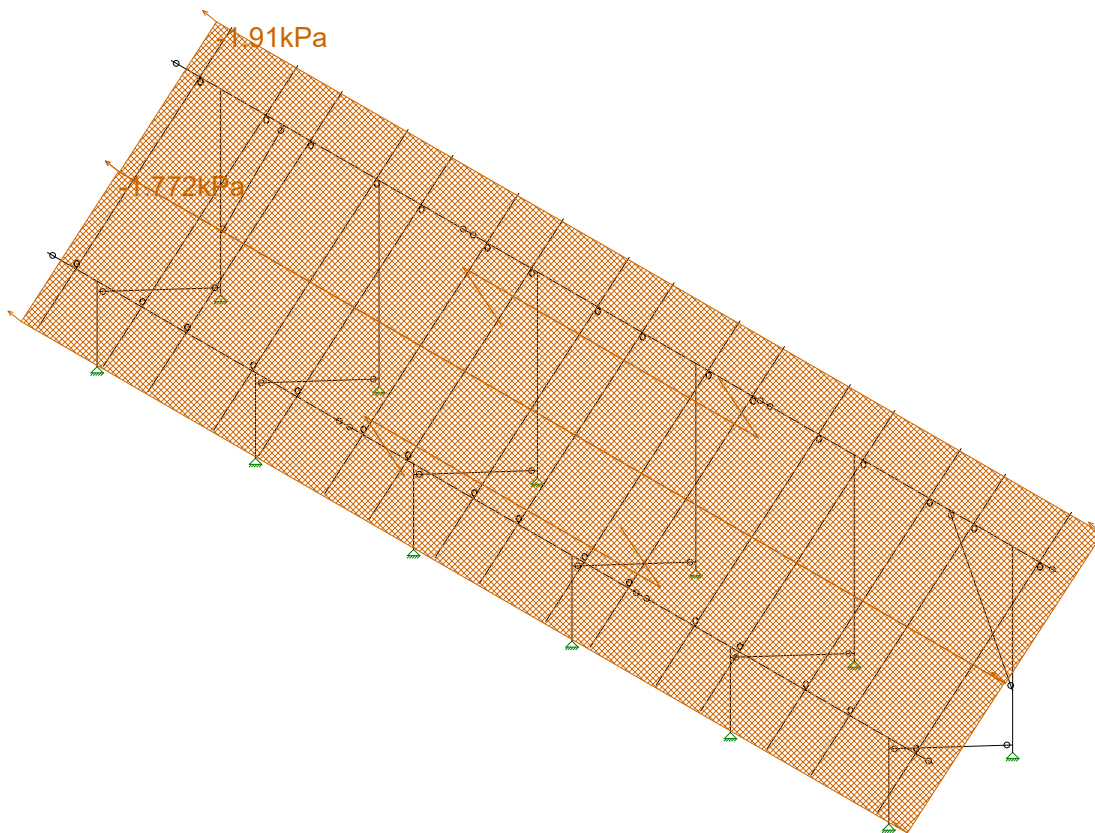
Loads: BLC 4, Wind A 0 deg
Envelope Only Solution

Vector Structural Engineeri..	BC Ground Mount	SK - 10
STB		Feb 14, 2019 at 12:12 PM
U2716.072.181		BC GM 40 deg (2-12-19).r3d



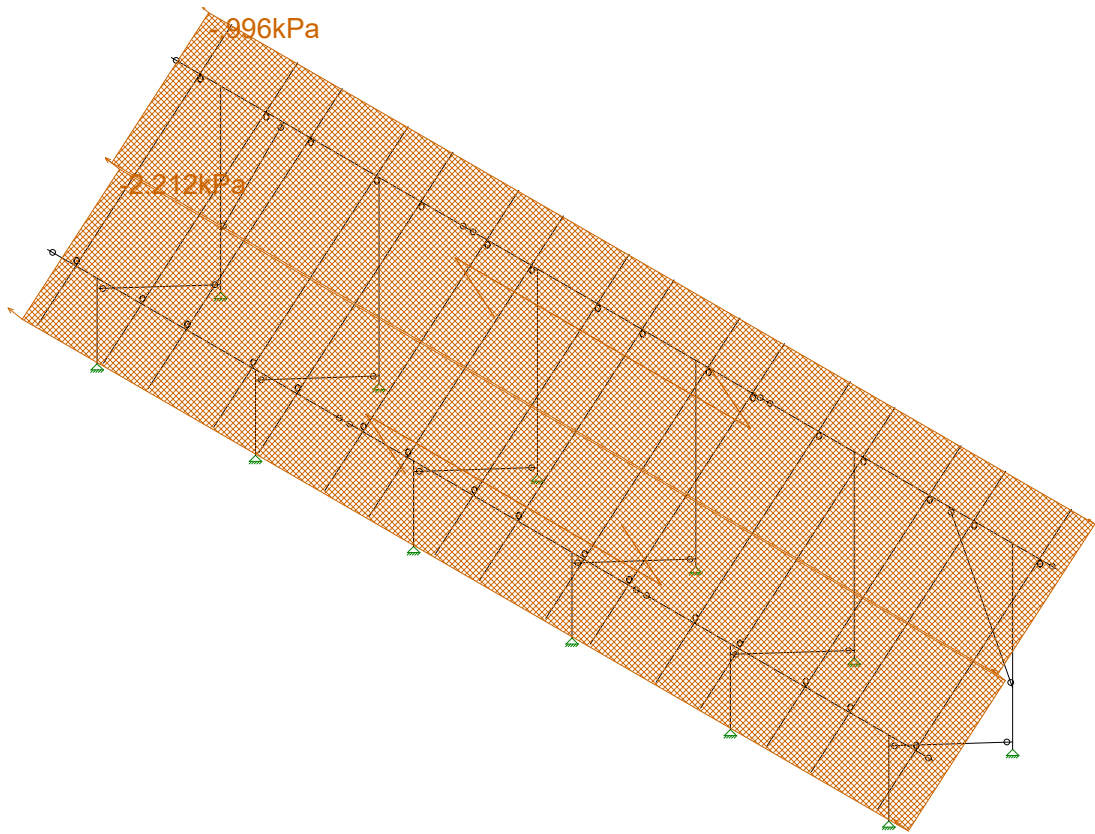
Loads: BLC 5, Wind B 0 deg
Envelope Only Solution

Vector Structural Engineeri..	BC Ground Mount	SK - 11
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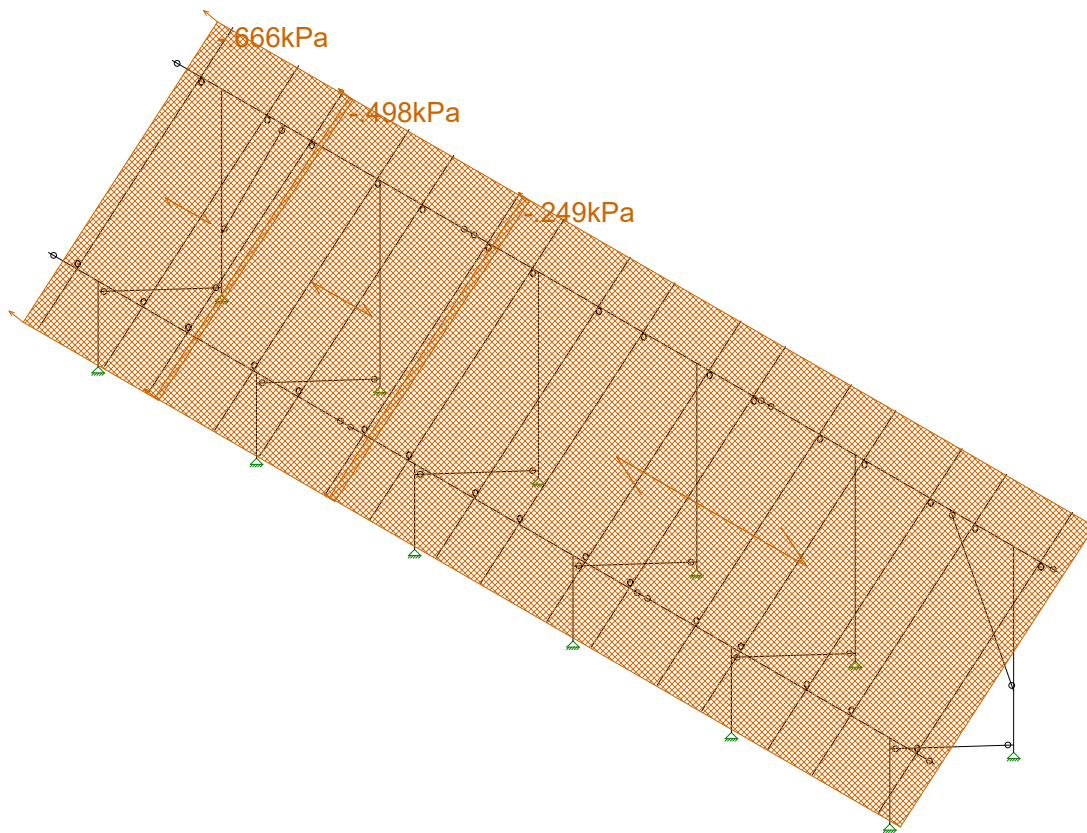
Loads: BLC 6, Wind A 180 deg
Envelope Only Solution

Vector Structural Engineeri..	BC Ground Mount	SK - 13
STB		Feb 14, 2019 at 12:12 PM
U2716.072.181		BC GM 40 deg (2-12-19).r3d



Loads: BLC 7, Wind B 180 deg
Envelope Only Solution

Vector Structural Engineeri..	BC Ground Mount	SK - 15
STB		Feb 14, 2019 at 12:12 PM
U2716.072.181		BC GM 40 deg (2-12-19).r3d



Loads: BLC 8, Wind A 90
Envelope Only Solution

Vector Structural Engineeri..

STB

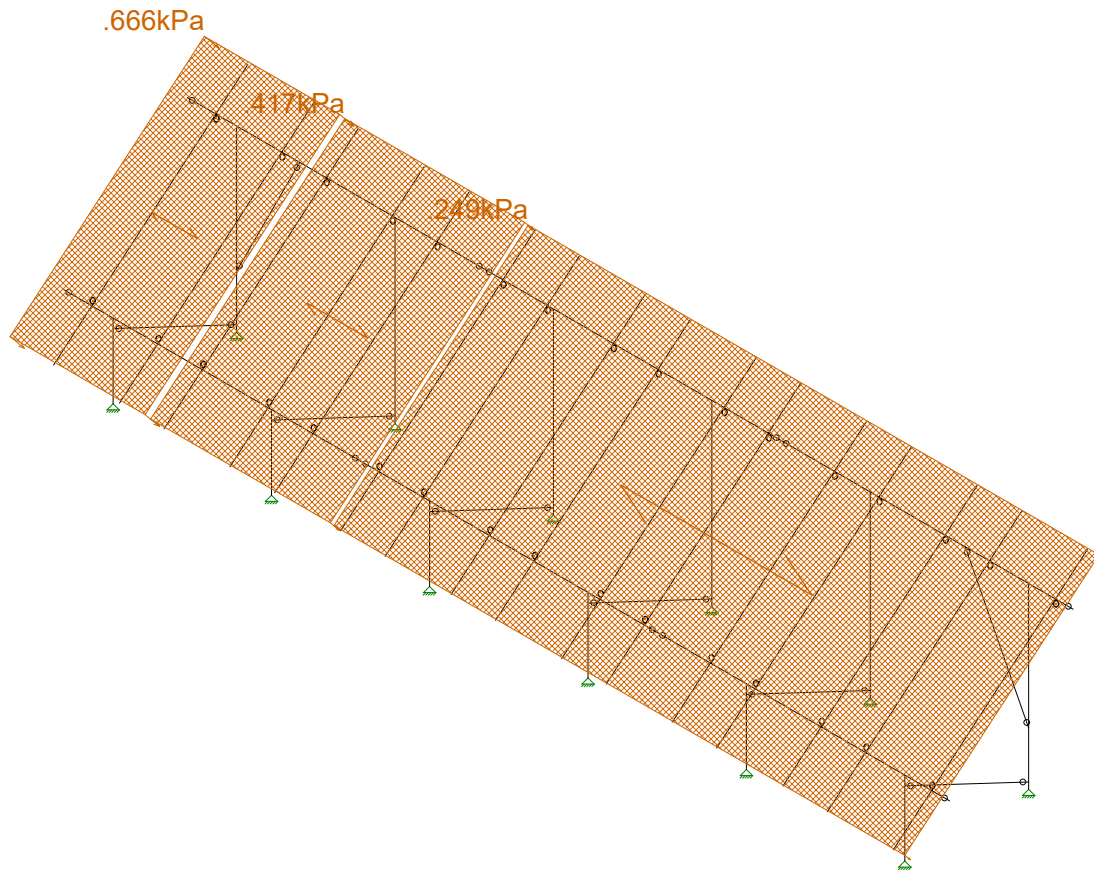
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BC Ground Mount

SK - 16

Feb 14, 2019 at 12:12 PM

BC GM 40 deg (2-12-19).r3d



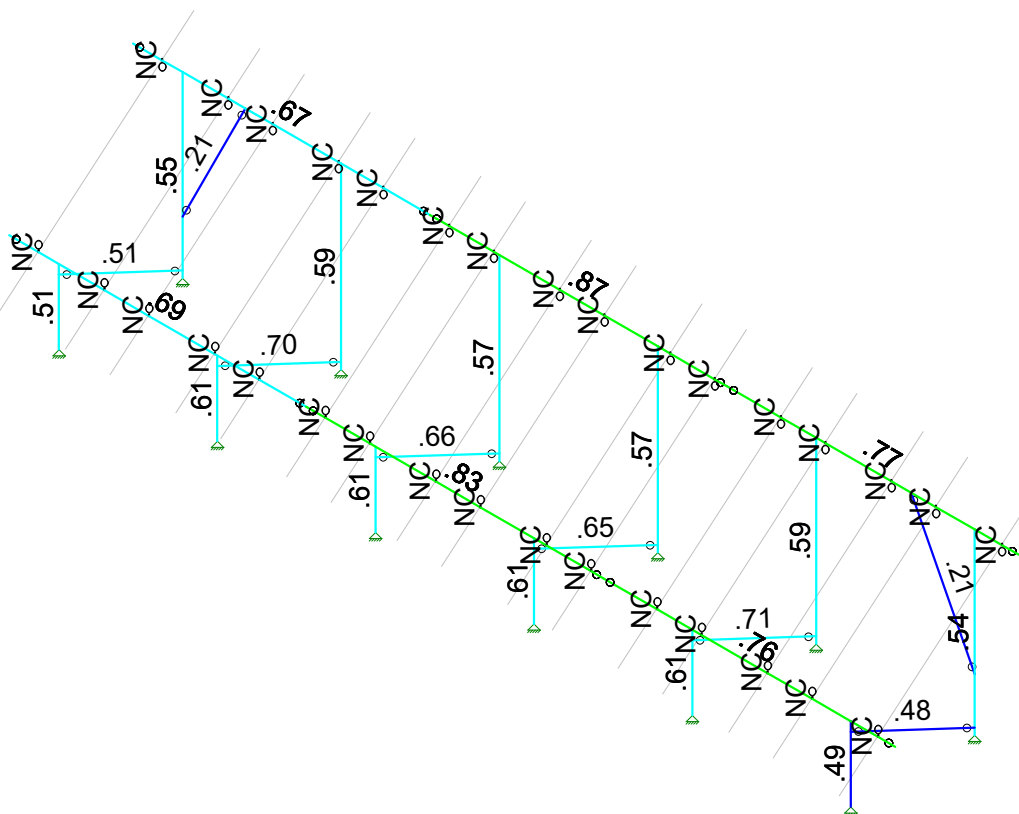
Loads: BLC 9, Wind B 90
Envelope Only Solution

Vector Structural Engineeri..	BC Ground Mount	SK - 17
STB		Feb 14, 2019 at 12:12 PM
U2716.072.181		BC GM 40 deg (2-12-19).r3d



Code Check
(Elem.)

Black	No Calc
Red	> 1.0
Yellow	40-1.0
Green	75-90
Cyan	50-75
Blue	0-.50

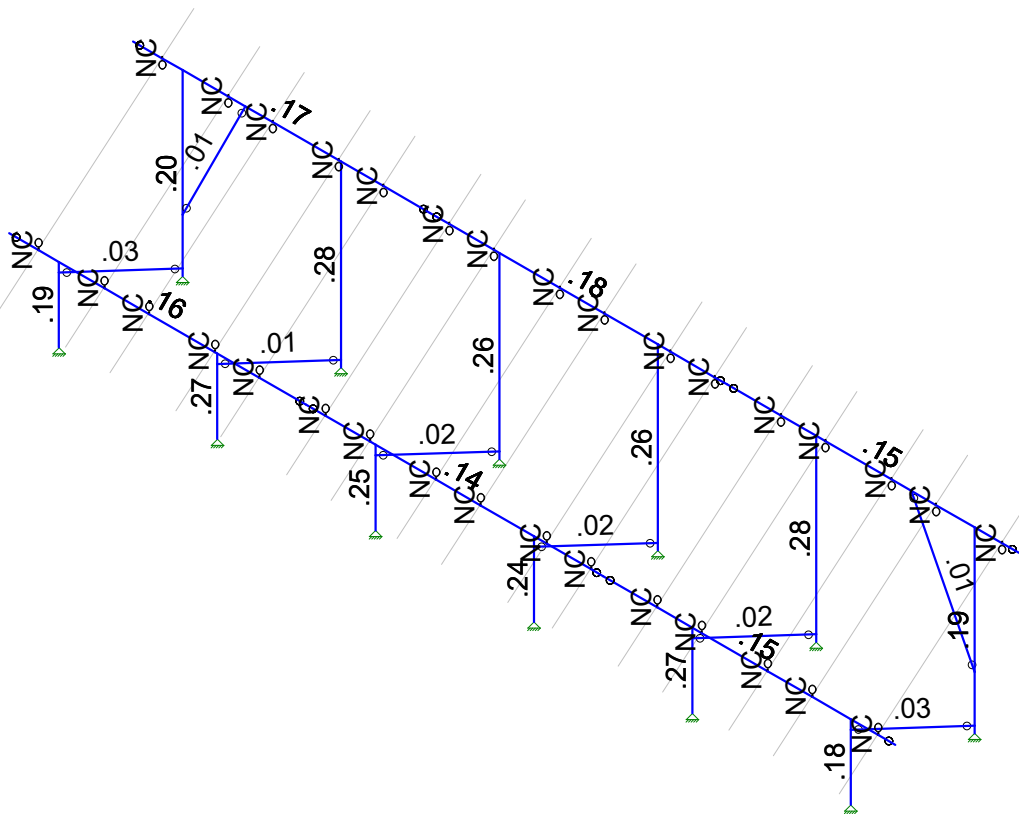


Member Code Checks Displayed (Enveloped)
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Vector Structural Engineeri...	BC Ground Mount	SK - 4
STB		Feb 14, 2019 at 12:10 PM
U2716.072.181		BC GM 40 deg (2-12-19).r3d



Shear Check
(Enr)
No Calc
> 1.0
40-1.0
75-50
50-75
0-.50



Member Shear Checks Displayed (Enveloped)
Envelope Only Solution

Vector Structural Engineeri...	BC Ground Mount	SK - 5
STB		Feb 14, 2019 at 12:10 PM
U2716.072.181		BC GM 40 deg (2-12-19).r3d



Company : Vector Structural Engineering
 Designer : STB
 Job Number : U2716.072.181
 Model Name : BC Ground Mount

Feb 14, 2019
 12:13 PM
 Checked By: _____

Aluminum Section Sets

	Label	Shape	Type	Design List	Material	Design R...	A [mm2]	Iyy [mm4]	Izz [mm4]	J [mm4]
1	AL Posts	2.375ODX0.188	Column	Pipe	6005-T5	Typical	832.26	3.238e+5	3.238e+5	6.41e+5
2	AL Brace	RT1.5x2x0.15625	VBrace	Rectangular Tubes	6005-T5	Typical	642.643	1.361e+5	2.183e+5	2.505e+5
3	AL Rails	HR250 ALA	Beam	Rectangular Tubes	6005-T5	Typical	466.453	39542.3...	2.023e+5	1.086e+5
4	AL Cross Beam	Cross Rail	Beam	Rectangular Tubes	6005-T5	Typical	1231.615	8.2e+5	1.817e+6	1.672e+6

Member Area Loads (BLC 2 : Solar Panel Weight)

	Joint A	Joint B	Joint C	Joint D	Direction	Distribution	Magnitude[kPa]
1	N197	N200	N199	N196	Y	A-B	-.12

Member Area Loads (BLC 3 : Roof Live/Snow)

	Joint A	Joint B	Joint C	Joint D	Direction	Distribution	Magnitude[kPa]
1	N197	N200	N199	N196	PY	A-B	-2.011

Member Area Loads (BLC 4 : Wind A 0 deg)

	Joint A	Joint B	Joint C	Joint D	Direction	Distribution	Magnitude[kPa]
1	N197	N200	N201	N198	Perp	A-B	1.436
2	N198	N201	N199	N196	Perp	A-B	1.494

Member Area Loads (BLC 5 : Wind B 0 deg)

	Joint A	Joint B	Joint C	Joint D	Direction	Distribution	Magnitude[kPa]
1	N197	N200	N201	N198	Perp	A-B	1.963
2	N198	N201	N199	N196	Perp	A-B	.527

Member Area Loads (BLC 6 : Wind A 180 deg)

	Joint A	Joint B	Joint C	Joint D	Direction	Distribution	Magnitude[kPa]
1	N197	N200	N201	N198	Perp	A-B	-1.91
2	N198	N201	N199	N196	Perp	A-B	-1.772

Member Area Loads (BLC 7 : Wind B 180 deg)

	Joint A	Joint B	Joint C	Joint D	Direction	Distribution	Magnitude[kPa]
1	N197	N200	N201	N198	Perp	A-B	-.996
2	N198	N201	N199	N196	Perp	A-B	-2.212

Member Area Loads (BLC 8 : Wind A 90)

	Joint A	Joint B	Joint C	Joint D	Direction	Distribution	Magnitude[kPa]
1	N197	N203	N202	N196	Perp	A-B	-.666
2	N203	N209	N208	N202	Perp	A-B	-.498
3	N209	N200	N199	N208	Perp	A-B	-.249

Member Area Loads (BLC 9 : Wind B 90)

	Joint A	Joint B	Joint C	Joint D	Direction	Distribution	Magnitude[kPa]
1	N197	N203	N202	N196	Perp	A-B	.666
2	N203	N209	N208	N202	Perp	A-B	.417
3	N209	N200	N199	N208	Perp	A-B	.249

Basic Load Cases

	BLC Description	Category	X Gravity	Y Gravity	Z Gravity	Joint	Point	Distributed	Area(M... Surface...
1	Self Weight	DL		-1.05					
2	Solar Panel Weight	DL							1



JOB NO.: U2716-071-181

DESIGNED: STB

PROJECT: Ground Mount Package for Alberta Canada

HR250 Rail Analysis

Envelope Maximum Member Section Forces

Member	Axial[...]	Loc[...]	LC y	Shear[...]	Loc[...]	LC z	Shear[...]	Loc[...]	LC Torque[...]	Loc[...]	LC y-y Mome[...]	Loc[...]	LC z-z Mome[...]	Loc[...]	LC
1	M16	m..2.648	813...11	1.846	813...9	0	0	9	.002	813...3	.002	325...17	.484	772...9	9
2		min-2.375	325...10	-1.883	325...10	0	329...11	-0.002	813...17	-0.001	325...3	-.749	211...10	10	
3	M25	m..2.089	813...11	1.87	813...9	0	0	2	.002	813...2	0	325...18	.527	207...17	17
4		min-1.964	325...10	-1.96	325...10	0	813...2	-0.001	813...18	-0.001	325...2	-.766	215...10	10	
5	M28	m..773	813...2	1.774	813...9	0	813...2	0	813...18	0	325...2	.481	207...17	17	
6		min-1.464	325...2	-1.795	325...10	0	329...2	0	813...2	0	325...18	-.741	207...9	9	
7	M31	m..4.425	813...5	1.76	813...9	0	813...2	0	813...17	.001	325...9	.523	203...17	17	
8		min-4.227	325...4	-1.814	325...10	0	329...2	-0.001	813...9	0	325...17	-.762	211...10	10	
9	M40	m..1.263	813...11	1.774	813...9	0	813...10	0	813...17	.002	325...4	.486	207...17	17	
10		min-1.296	325...10	-1.797	325...10	0	329...10	-0.002	813...4	0	325...17	-.741	211...10	10	
11	M43	m..1.259	813...10	1.777	813...9	0	0	10	.002	813...4	0	325...17	.478	207...17	17
12		min-1.097	325...2	-1.791	325...10	0	813...10	0	813...17	-0.002	325...4	-.737	207...9	9	
13	M64	m..4.458	813...5	1.759	813...9	0	0	10	.002	813...10	0	325...17	.524	203...17	17
14		min-4.465	325...4	-1.816	325...10	0	813...10	0	813...17	-0.002	325...10	-.764	211...10	10	
15	M67	m..1.033	813...11	1.774	813...9	0	0	2	0	813...11	0	325...16	.484	207...17	17
16		min-1.224	325...2	-1.796	325...10	0	329...10	0	813...16	0	325...11	-.741	207...9	9	
17	M112	m..1.527	813...11	1.771	813...9	0	0	10	0	813...16	0	325...11	.49	207...17	17
18		min-1.602	325...10	-1.799	325...10	0	329...2	0	813...11	0	325...16	-.744	211...10	10	
19	M115	m..4.255	813...5	1.76	813...9	0	813...10	.001	813...17	.002	325...10	.522	203...17	17	
20		min-4.309	325...4	-1.815	325...10	0	329...10	-0.002	813...4	-0.001	325...17	-.763	211...10	10	
21	M208	m..1.54	813...10	1.778	813...9	0	813...10	0	813...17	.002	325...4	.475	207...17	17	
22		min-1.321	325...11	-1.788	325...10	0	329...10	-0.002	813...4	0	325...17	-.736	207...9	9	
23	M211	m..1.887	813...11	1.771	813...9	0	0	10	.002	813...4	0	325...17	.493	207...17	17
24		min-1.828	325...10	-1.8	325...10	0	813...10	0	813...17	-0.002	325...4	-.746	211...10	10	
25	M400	m..4.064	813...11	1.761	813...9	0	0	2	.001	813...2	0	325...18	.519	203...17	17
26		min-3.793	325...4	-1.812	325...10	0	813...2	0	813...18	-0.001	325...2	-.76	211...10	10	
27	M403	m..65	813...2	1.774	813...9	0	0	2	0	813...2	0	325...18	.479	207...17	17
28		min-1.588	325...2	-1.795	325...10	0	329...14	0	813...18	0	325...2	-.741	207...9	9	
29	M784	m..2.471	813...11	1.851	813...9	0	813...2	.001	813...18	.002	325...2	.59	207...17	17	
30		min-2.045	325...10	-1.891	325...10	0	329...2	-0.002	813...2	-0.001	325...18	-.799	211...10	10	
31	M787	m..2.094	813...11	1.532	813...9	0	0	11	.002	813...17	.002	325...3	.388	203...17	17
32		min-1.909	325...10	-1.55	325...10	0	329...9	-0.002	813...3	-0.002	325...17	-.649	207...9	9	

Title: HR 250

Purpose: Determine the flexural and shear capacity of the aluminum extrusion.

References:

2015 Aluminum Design Manual

Assumptions & Limitations:

1. The shape is loaded in plane parallel to a principle axis that passes through the shear center, or the shape is restrained against rotation about the longitudinal axis at load points and supports.
 2. The aluminum is a wrought (not cast) product.
 3. The beams ends are prevented from lateral deflection and axial rotation, but are free to rotate about the vertical axis.
 4. The shape is not welded.
 5. The shape has flat webs that are supported on both edges.
-

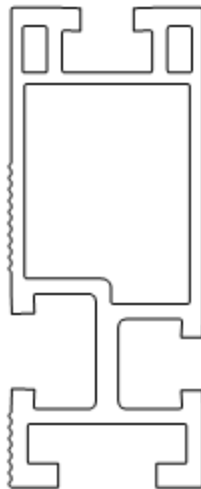
Input:

Shape Name = HR 250

Material = 6005-T5

$L_b := 8.083 \text{ ft}$

(beam unbraced length, rupture controls up to an unbraced length of 4.75 ft, then lateral-torsional buckling will control)



Material Properties:

$$E := 10100 \text{ ksi}$$

(highlighted items change based on the temper)

(modulus of elasticity, Table A.3.1)

$$F_{ty} := 35 \text{ ksi}$$

(tensile yield strength, Table A.3.3)

$$F_{tu} := 38 \text{ ksi}$$

(tensile ultimate strength, Table A.3.3)

$$k_t := 1.25$$

(tension coefficient, Table A.3.3)

$$F_{cy} := F_{ty} = 35 \text{ ksi}$$

(compressive yield strength, Table A.3.1; not always = F_{ty})

$$F_{sy} := 0.6 \cdot F_{ty} = 21 \text{ ksi}$$

(shear yield strength, Table A.3.1)

$$F_{su} := 0.6 \cdot F_{tu} = 22.8 \text{ ksi}$$

(shear ultimate strength, Table A.3.1)

Section Properties:

(highlighted items changed based on the shape)

$$Z := 0.521 \text{ in}^3$$

(plastic section modulus about strong axis; per RISASection)

$$I_x := 0.487 \text{ in}^4$$

(moment of inertia about strong axis per RISASection)

$$I_y := 0.095 \text{ in}^4$$

(moment of inertia about weak axis per RISASection)

$$S_t := 0.387 \text{ in}^3$$

(section modulus on the tension side of the neutral axis per RISASection)

$$S_c := 0.387 \text{ in}^3$$

(section modulus on the compression side of the neutral axis per RISASection)

$$S_{xc} := S_c = 0.387 \text{ in}^3$$

(section modulus on the compression side of the x-axis)

$$b := 1.1224 \text{ in}$$

(clear height of the web)

$$t := 0.07 \text{ in}$$

(web thickness)

$$n_w := 2$$

(# of webs)

$$d := 2.5 \text{ in}$$

(full depth of section per RISASection)

$$J_c := 0.091 \text{ in}^4$$

(torsion constant per RISASection)

Constants:

$$\kappa := 1.0 \text{ ksi}$$

(metric conversion factor, Tables B.4.1 & B.4.2)

F.2 Yielding & Rupture:

Yielding:

$$M_{np} := \min(Z \cdot F_{cy}, 1.5 \cdot S_t \cdot F_{ty}, 1.5 \cdot S_c \cdot F_{cy}) \quad (\text{nominal flexural strength})$$

$$M_{np} = 1.52 \text{ kip} \cdot \text{ft}$$

Rupture:

$$M_{nu} := \frac{Z \cdot F_{tu}}{k_t} \quad (\text{nominal flexural strength, Equation F.2-1})$$

$$M_{nu} = 1.32 \text{ kip} \cdot \text{ft}$$

F.3 Local Buckling:

$$F_b := 35 \text{ ksi} \quad (\text{see attached spreadsheet})$$

$$M_{nlb} := F_b \cdot S_{xc} = 1.129 \text{ kip} \cdot \text{ft} \quad (\text{nominal flexural strength})$$

F.4 Lateral-Torsional Buckling:

(highlighted equations change based on the temper)

$$B_c := F_{cy} \cdot \left(1 + \left(\frac{F_{cy}}{2250 \cdot \kappa} \right)^2 \right)^{\frac{1}{2}} = 39.365 \text{ ksi} \quad (\text{buckling constant intercept for member buckling, Table B.4.2})$$

$$D_c := \frac{B_c}{10} \cdot \left(\frac{B_c}{E} \right)^{\frac{1}{2}} = 0.246 \text{ ksi} \quad (\text{buckling constant slope for member buckling, Table B.4.2})$$

$$C_c := 0.41 \cdot \frac{B_c}{D_c} = 65.673 \quad (\text{buckling constant intersection for member buckling, Table B.4.2})$$

$$C_b := 1.0 \quad (\text{coefficient that accounts for the moment gradient along a beam's length, Section F.4.1; conservatively assume } C_b = 1.0)$$

$$\lambda := 2.3 \cdot \sqrt{\frac{L_b \cdot S_{xc}}{C_b \cdot \sqrt{I_y \cdot J_c}}} = 46.214 \quad (\text{slenderness, Equation F.4-6})$$

$$M_{nmbo} := M_{np} \cdot \left(1 - \frac{\lambda}{C_c} \right) + \frac{\pi^2 \cdot E \cdot \lambda \cdot S_{xc}}{C_c^3} = 0.975 \text{ kip} \cdot \text{ft} \quad (\text{nominal flexural strength if no part of the cross section is weld-affected})$$

$$M_{nmb} := M_{nmbo} = 0.975 \text{ kip} \cdot \text{ft} \quad (\text{nominal flexural strength for the limit state of lateral-torsional buckling})$$

Available Flexural Strength:

$$\phi_{bnp} := 0.90 \quad \phi_{bnu} := 0.75 \quad \phi_{bnlb} := 0.90 \quad \phi_{bnmb} := 0.90 \quad (\text{resistance factors, Section F.1})$$

$$\Omega_{np} := 1.65 \quad \Omega_{bnu} := 1.95 \quad \Omega_{bnlb} := 1.65 \quad \Omega_{bnmb} := 1.65 \quad (\text{safety factors, Section F.1})$$

LRFD Capacity:

$$M_u := \min(\phi_{bnp} \cdot M_{np}, \phi_{bnu} \cdot M_{nu}, \phi_{bnlb} \cdot M_{nlb}, \phi_{bnmb} \cdot M_{nmb}) = 1.189 \text{ kN} \cdot \text{m}$$

ASD Capacity:

$$M_a := \min\left(\frac{M_{np}}{\Omega_{np}}, \frac{M_{nu}}{\Omega_{bnu}}, \frac{M_{nlb}}{\Omega_{bnlb}}, \frac{M_{nmb}}{\Omega_{bnmb}}\right) = 0.801 \text{ kN} \cdot \text{m}$$

G.1 General Provisions:

Yielding & Shear Buckling:

(highlighted equations change based on the temper)

$$B_s := F_{sy} \cdot \left(1 + \left(\frac{F_{sy}}{800 \cdot \kappa} \right)^3 \right)^{\frac{1}{3}} = 27.241 \text{ ksi}$$

(buckling constant intercept for shear in flat elements, Table B.4.2)

$$D_s := \frac{B_s}{10} \cdot \left(\frac{B_s}{E} \right)^{\frac{1}{2}} = 0.141 \text{ ksi}$$

(buckling constant slope for shear in flat elements, Table B.4.2)

$$C_s := 0.41 \frac{B_s}{D_s} = 78.946$$

(buckling constant intersection for shear in flat elements, Table B.4.2)

$$\lambda_1 := \frac{B_s - F_{sy}}{1.25 \cdot D_s} = 35.292$$

(slenderness at the intersection of the equations for yielding and inelastic buckling, Section G.2)

$$\lambda_2 := \frac{C_s}{1.25} = 63.157$$

(slenderness at the intersection of the equations for inelastic buckling and elastic buckling, Section G.2)

$$\frac{b}{t} = 16.034$$

Since $b/t \leq \lambda_{1}$:

$$F_s := F_{sy} = 21 \text{ ksi}$$

(shear stress corresponding to the shear strength, Section G.2; equation changes based on b/t)

$$F_{so} := F_s = 21 \text{ ksi}$$

(shear stress corresponding to the unwelded shear strength)

$$A_v := d \cdot t \cdot n_w = 0.35 \text{ in}^2$$

(web area, Equation G.2-3)

$$V_{n1} := F_{so} \cdot A_v = 7.35 \text{ kip}$$

(nominal shear strength, Equation G.1-1)

G.2 Members with Flat Webs Supported on Both Edges:

Rupture:

$$A_n := A_v = 0.35 \text{ in}^2$$

(net area of the web)

$$V_{n2} := \frac{F_{su} \cdot A_n}{k_t} = 6.384 \text{ kip}$$

(nominal shear strength, Equation G.2-1)

Available Shear Strength:

$$\phi_{v1} := 0.90 \quad \phi_{v2} := 0.75 \quad \Omega_{v1} := 1.65 \quad \Omega_{v2} := 1.95$$

(resistance & safety factors, Section G.1)

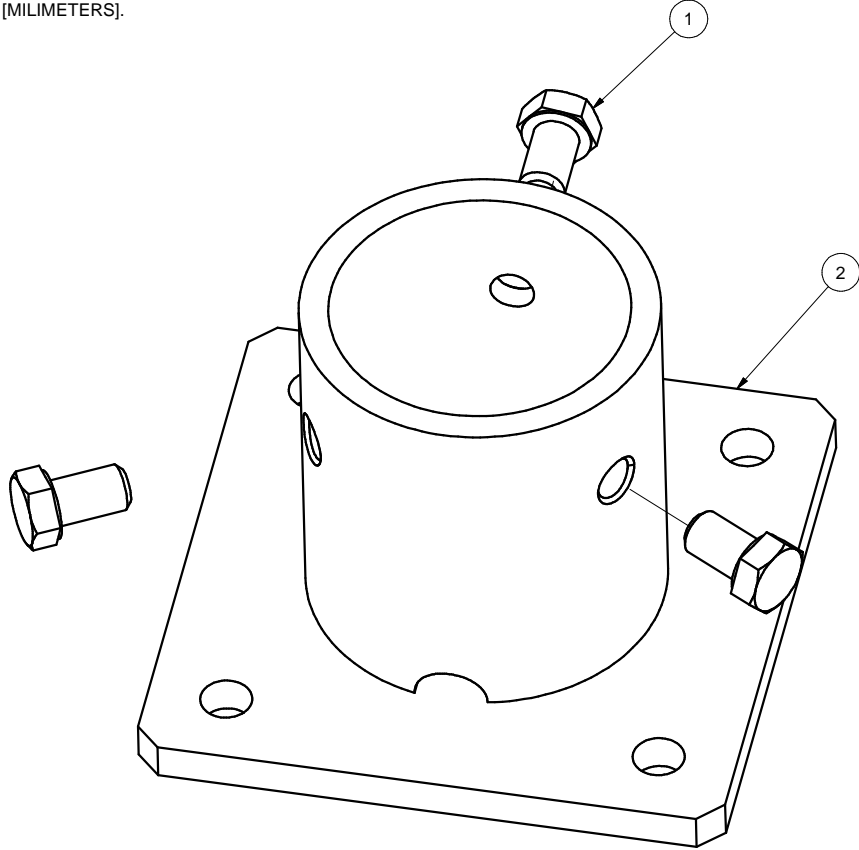
LRFD Capacity:

$$V_u := \min(\phi_{v1} \cdot V_{n1}, \phi_{v2} \cdot V_{n2}) = 21.298 \text{ kN}$$

ASD Capacity:

$$V_a := \min\left(\frac{V_{n1}}{\Omega_{v1}}, \frac{V_{n2}}{\Omega_{v2}}\right) = 14.563 \text{ kN}$$

NOTES: UNLESS OTHERWISE SPECIFIED
 1. DIMENSIONS SHOWN ARE INCHES [MILLIMETERS].



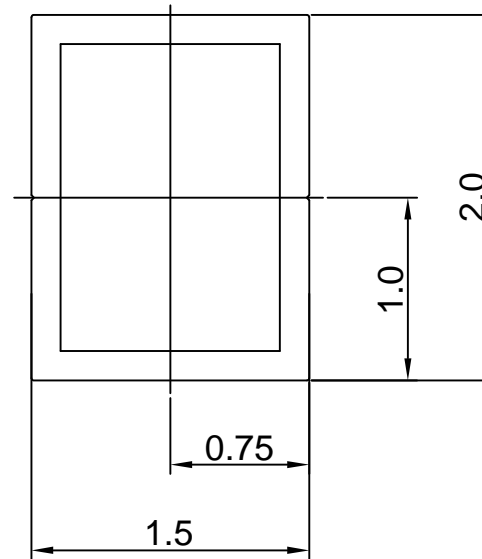
REVISIONS			
REV	DESCRIPTION	BY	DATE
A	INITIAL RELEASE	LWF	10/20/2016

2	A21120-001	2" PIPE BASE	1
1	B15018-011	HEX CAP SCREW 3/8-16 X 5/8	3
ITEM	PART NUMBER	DESCRIPTION	QTY
MATERIAL		SEE NOTES	
Third Angle Projection:			
GENERAL SPECIFICATIONS		Sunmodo Corp. 1905 E 5TH STREET, STE A, VANCOUVER, WA 98661	
All Dimensions in inches [millimeters] Tolerances X.XXX ±0.01 [0.25mm] X.XX ±0.02 [0.50mm] X.X ±0.039 [1.0mm] Unless otherwise spec'd		Break all sharp edges .010-.020 unless otherwise specified.	
DRAWN BY		TITLE	
LWF		2" PIPE BASE KIT	
CHECKED BY		DRAWING NUMBER	
		B K10268-001	
APPROVALS		SCALE: NONE SHEET 1 of 1	

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NOTES: UNLESS OTHERWISE SPECIFIED

1. DIMENSIONS SHOWN ARE INCHES [MILIMETERS].
2. MATERAIL: ALUMINUM 6005-T5.
FINISH: CLEAR ANODIZED 10 μ m THICK.
3. THE UNSPECIFIED DIMENSIONS ARE SPECIFIED BY 2D CAD FILE.



Section properties:

Weight: 1.156 lbs/ft

Area: 0.992 in²

Perimeter: 12.601 in

Bounding Box: X: -1.000,1.000

Y: -0.750, 0.750

Centroid:(0.000,0.000)

Moments of Inertia(in⁴): I_x=0.506,I_y=0.322

Section modulus in bending(in³): W_x=0.675,W_y=0.322

Radii of Gyration: X: 0.714, Y: 0.570

MATERIAL		SEE NOTES	
Third Angle Projection:			
GENERAL SPECIFICATIONS			
All Dimensions in inches [millimeters]			
Tolerances			
X.XXX ± 0.01 [0.25mm]		Break all sharp edges	
X.XX ± 0.02 [0.50mm]		.010-.020 unless	
X.X ± 0.039 [1.0mm]		otherwise specified.	
Unless otherwise specd			
DRAWN BY	DATE		
zcg	03/12/2014		
CHECKED BY		B	DRAWING NUMBER
			A20164
APPROVALS		SCALE:	NONE
		SHEET	1 of 1

Sunmodo Corp.

1905 E 5TH STREET, SUITE A, VANCOUVER, WA 98661

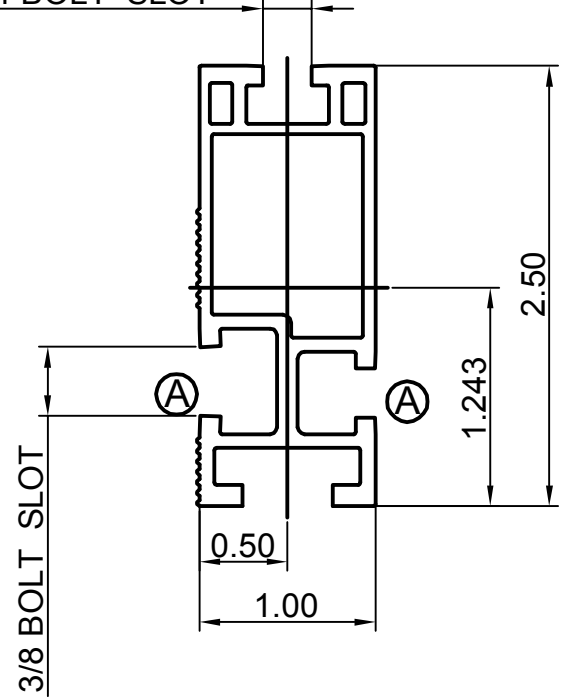
TITLE
1.5X2 AL TUBE BRACE EXTRUSION

REVISIONS			
REV	DESCRIPTION	BY	DATE
A	ADDED BOTTOM CHANNEL & CHANGED ONE 3/8 CHANNEL TO 1/4	zcg	02/21/2013

NOTES: UNLESS OTHERWISE SPECIFIED

1. DIMENSIONS SHOWN ARE INCHES [MILIMETERS].
2. MATERAIL: ALUMINUM 6005-T5.
FINISH: CLEAR ANODIZED 15 μ m THICK.
3. THE UNSPECIFIED DIMENSIONS ARE SPECIFIED BY 2D CAD FILE.

2X 1/4 BOLT SLOT



Section properties:

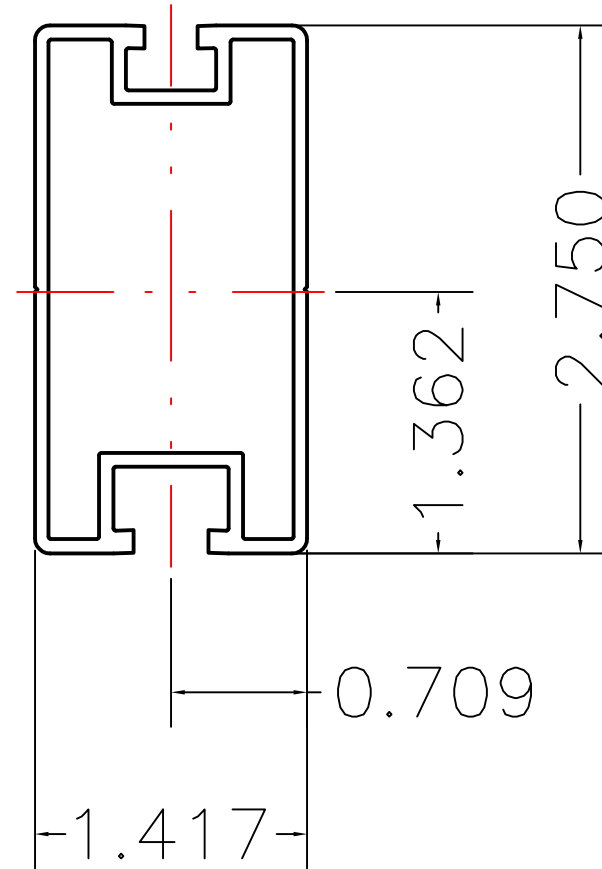
Weight: 0.850 lbs/ft
 Area: 0.723 in²
 Perimeter: 17.325 in
 Bounding Box: X: -0.500,0.500
 Y: -1.243,1.257

Centroid:(0.000,0.000)
 Moments of Inertia(in⁴): Ix=0.486,Iy=0.095
 Section modulus in bending(in³): Wx=0.387,Wy=0.190
 Radii of Gyration: X: 0.820, Y: 0.363

MATERIAL SEE NOTES		Sunmodo Corp.	
Third Angle Projection:			
GENERAL SPECIFICATIONS All Dimensions in inches [millimeters]		1905 E 5TH STREET, SUITE A, VANCOUVER, WA 98661	
Tolerances: X.XXX ± 0.01 [0.25mm] X.XX ± 0.02 [0.50mm] X.X ± 0.039 [1.0mm] Unless otherwise spec'd		TITLE HELIO STANDARD RAIL	
DRAWN BY zcg	DATE 02/21/2013	DRAWING NUMBER A20144	
CHECKED BY		SCALE: NONE SHEET 1 of 1	
APPROVALS			

NOTES: UNLESS OTHERWISE SPECIFIED

1. DIMENSIONS SHOWN ARE INCHES [MILIMETERS].
2. MATERIAL: 6005-T5.
FINISH: CLEAR ANODIZED 10um THICK.
3. THE UNSPECIFIED RADII ARE .02" MAX.
4. THE UNSPECIFIED DIMENSIONS ARE SPECIFIED BY 2D CAD FILE.



Section properties:

Weight: 0.862 lbs/ft
 Area: 0.736 in²
 Perimeter: 19.824 in
 Bounding Box: X: -0.709,0.709
 Y: -1.362,1.388
 Centroid:(0.000,0.000)
 Moments of Inertia(in⁴): I_x=0.727,I_y=0.214
 Section modulus in bending(in³): W_x=0.524,W_y=0.302
 Radii of Gyration: X: 994, Y: 0.539

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MATERIAL SEE NOTES	
Third Angle Projection:	
GENERAL SPECIFICATIONS All Dimensions in inches [millimeters]	
Tolerances	
X.XXX ±0.01 [0.25mm]	Break all sharp edges
X.XX ±0.02 [0.50mm]	.010-.020 unless
X.X ±0.039 [1.0mm]	otherwise specified.
Unless otherwise spec'd	
DRAWN BY KYY	DATE 01/18/2018
CHECKED BY	
APPROVALS	

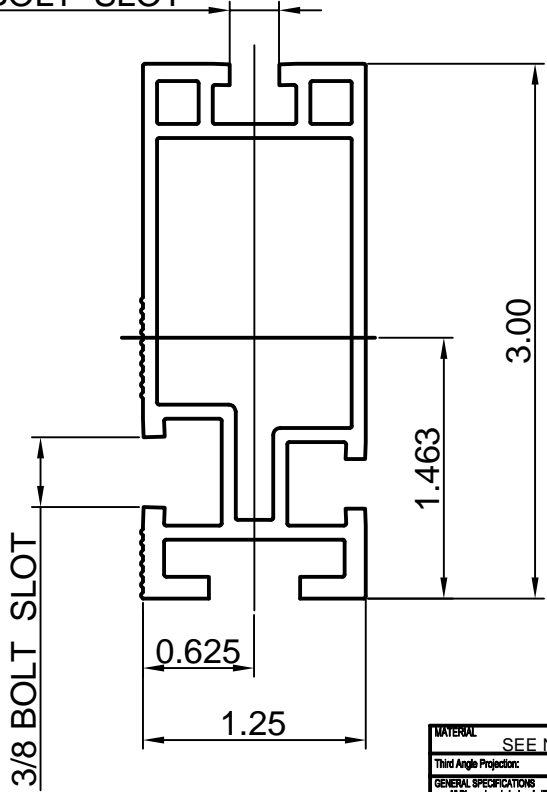
SunModo Corp.	
14800 NE 65TH STREET, VANCOUVER WA 98682	
TITLE RAIL, HR300 (SUNRAY), EXTRUSION	
B	DRAWING NUMBER A20288
SCALE: NONE	SHEET 1 of 1

REV	DESCRIPTON	BY	DATE
A	0.44 WAS 0.41, 0.44 WAS 0.33	LWF	11/30/2015

NOTES: UNLESS OTHERWISE SPECIFIED

1. DIMENSIONS SHOWN ARE INCHES [MILIMETERS].
2. MATERAIL: ALUMINUM 6005-T5.
FINISH: CLEAR ANODIZED 15 μ m THICK.
3. THE UNSPECIFIED DIMENSIONS ARE SPECIFIED BY 2D CAD FILE.

2X 1/4 BOLT SLOT



Section properties:

Weight: 1.151 lbs/ft
 Area: 0.980 in²
 Perimeter: 22.104 in
 Bounding Box: X: -0.625,0.625
 Y: -1.463,1.537
 Centroid:(0.000,0.000)
 Moments of Inertia(in⁴): Ix=1.047,Iy=0.207
 Section modulus in bending(in³): Wx=0.681,Wy=0.331
 Radii of Gyration: X: 1.034, Y: 0.460

MATERIAL		SEE NOTES	
Third Angle Projection			
GENERAL SPECIFICATIONS			
All Dimensions in Inches (millimeters)			
Tolerances			
XXX ±0.01 (0.25mm)			
XX ±0.02 (0.50mm)			
X ±0.03 (1.0mm)			
Unless otherwise specified.			
Break all sharp edges 0.10-0.25 unless otherwise specified.			
DRAWN BY		DATE	
ZCJ		02/21/2013	
CHECKED BY		B	
APPROVALS		DRAWING NUMBER	
		A20145	
SCALE:		SHEET	
NONE		1 of 1	

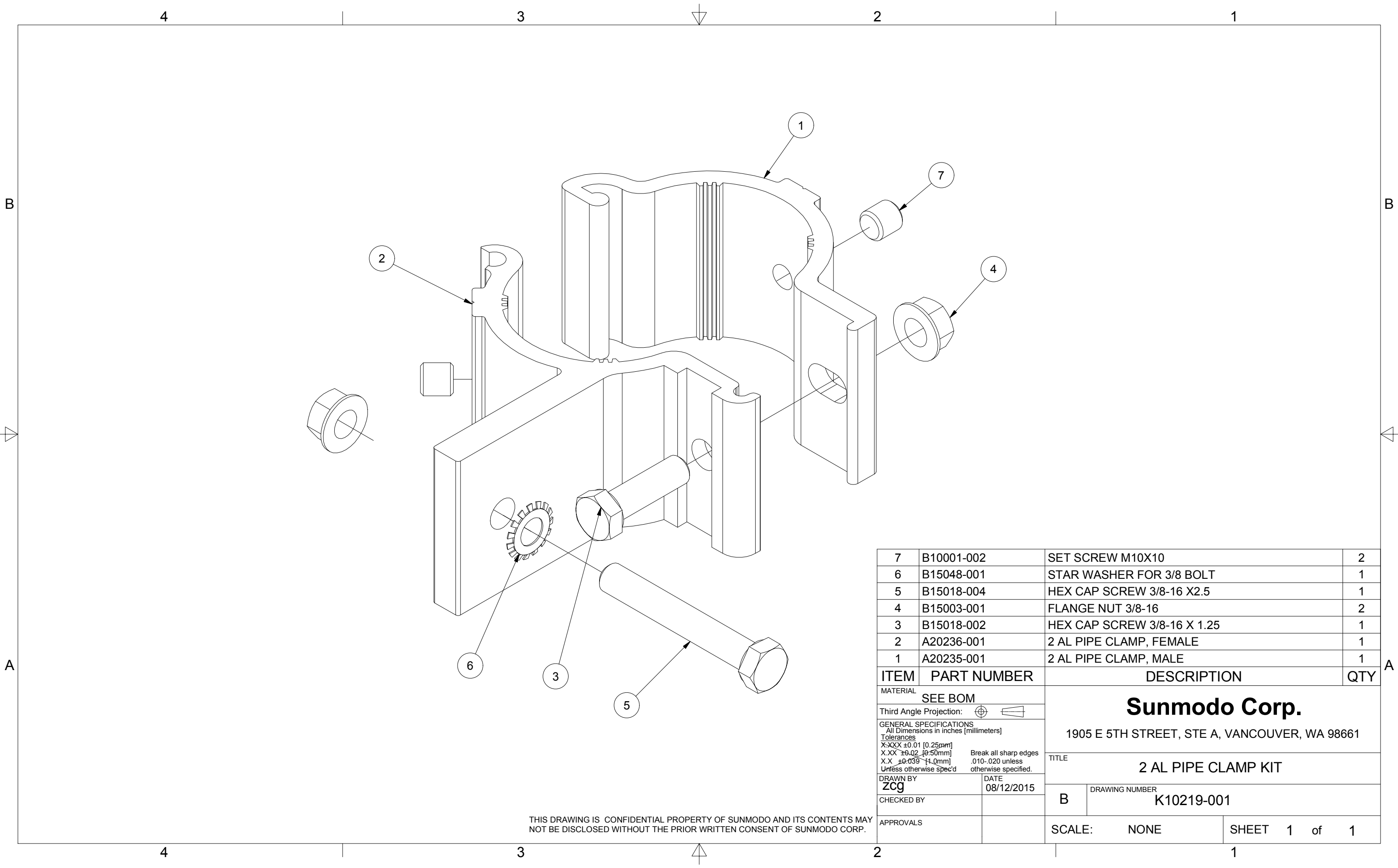
Sunmodo Corp.

1905 E 5TH STREET, SUITE A, VANCOUVER, WA 98661

TITLE
HELIO HEAVY RAIL

B DRAWING NUMBER
A20145

SCALE: NONE SHEET 1 of 1



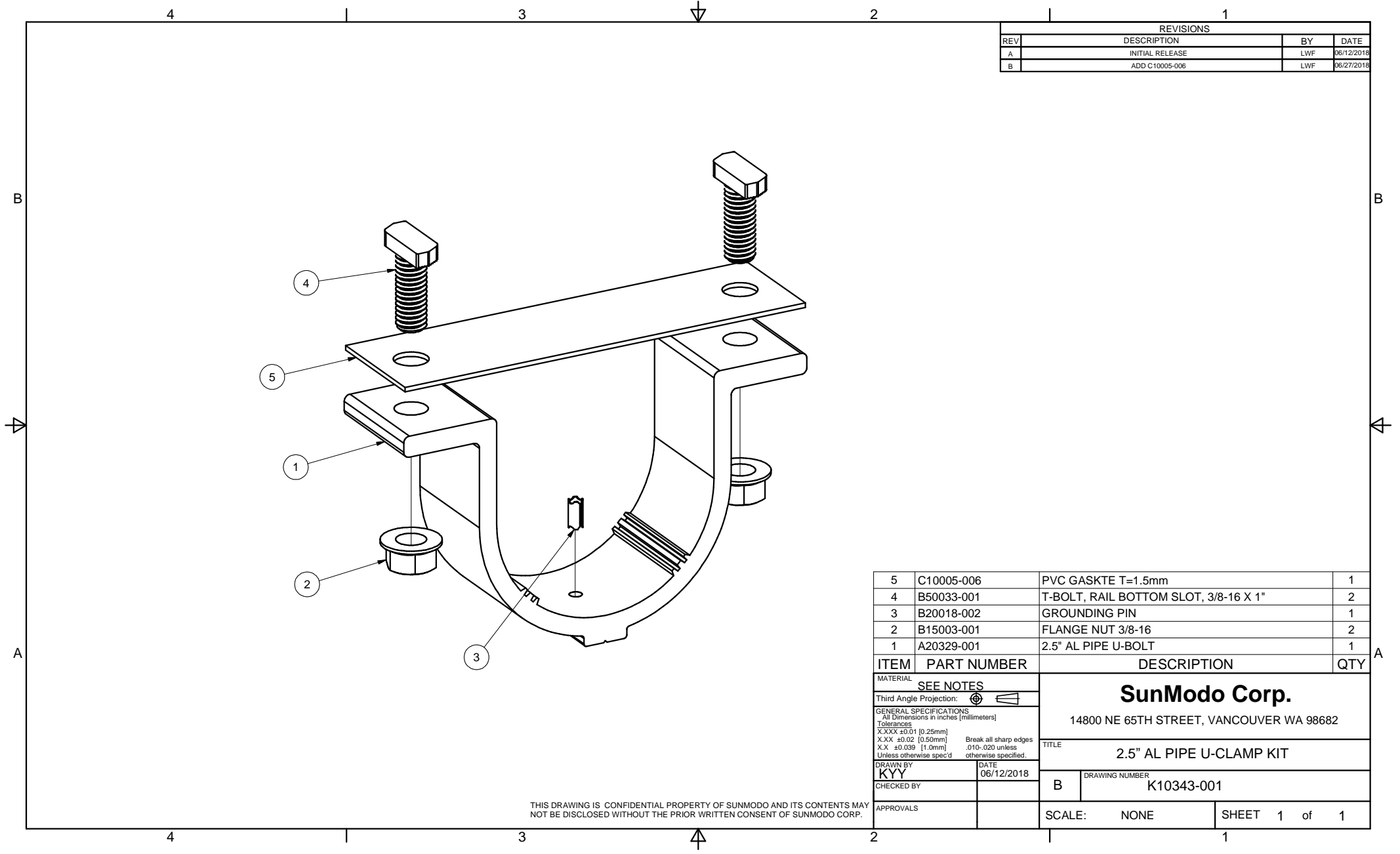
7	B10001-002	SET SCREW M10X10	2
6	B15048-001	STAR WASHER FOR 3/8 BOLT	1
5	B15018-004	HEX CAP SCREW 3/8-16 X2.5	1
4	B15003-001	FLANGE NUT 3/8-16	2
3	B15018-002	HEX CAP SCREW 3/8-16 X 1.25	1
2	A20236-001	2 AL PIPE CLAMP, FEMALE	1
1	A20235-001	2 AL PIPE CLAMP, MALE	1

ITEM	PART NUMBER	DESCRIPTION	QTY
MATERIAL		SEE BOM	
Third Angle Projection:			
GENERAL SPECIFICATIONS All Dimensions in inches (millimeters)			
Tolerances			
X.XXX ±0.01 [0.25mm]		Break all sharp edges	
X.XX ±0.02 [0.50mm]		.010-.020 unless	
X.X ±0.039 [1.0mm]		otherwise specified.	
DRAWN BY		DATE	
zcg		08/12/2015	
CHECKED BY		B	
APPROVALS		DRAWING NUMBER	
		K10219-001	
SCALE:		NONE	SHEET 1 of 1

Sunmodo Corp.
1905 E 5TH STREET, STE A, VANCOUVER, WA 98661

TITLE
2 AL PIPE CLAMP KIT

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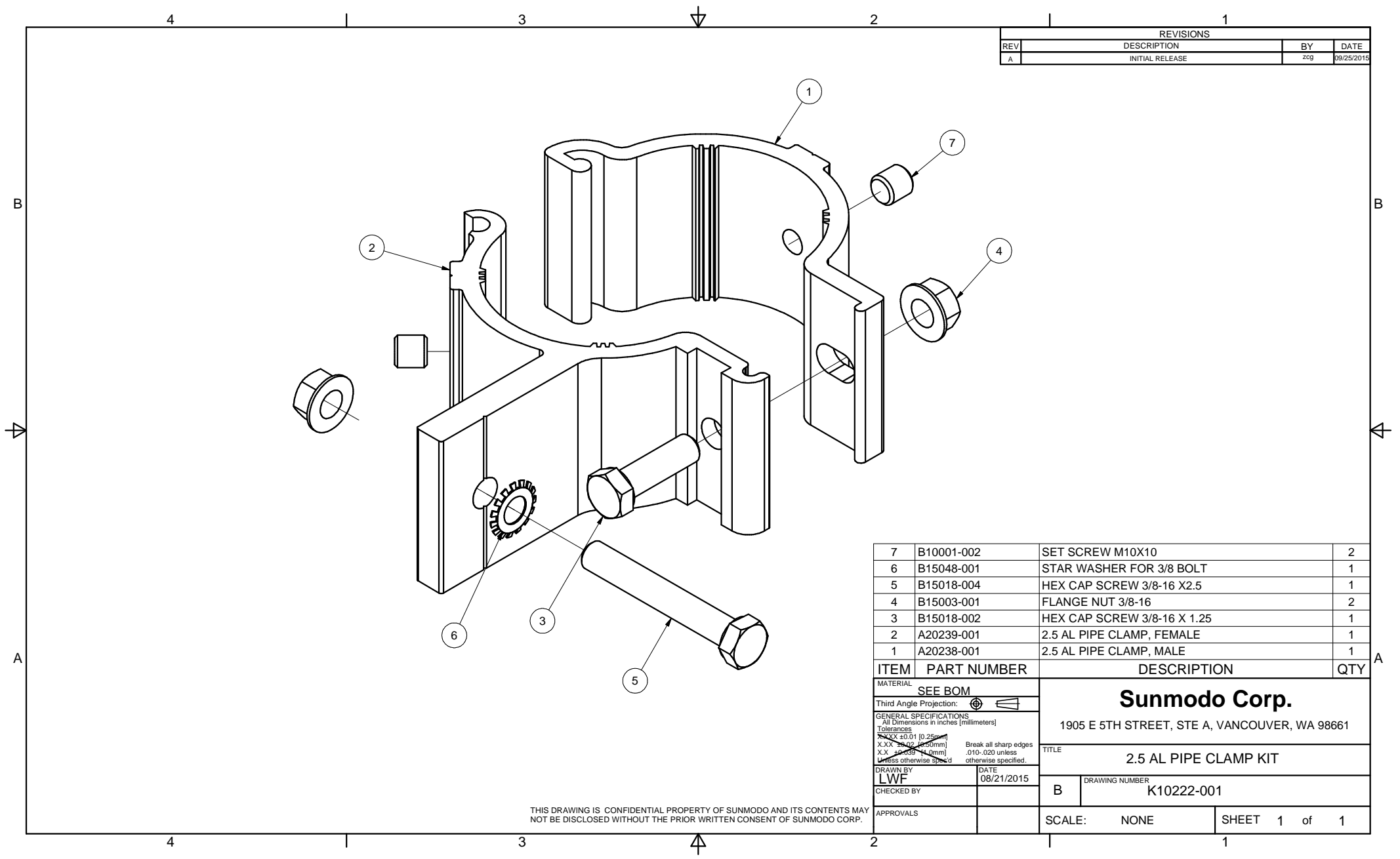


REVISIONS			
REV	DESCRIPTION	BY	DATE
A	INITIAL RELEASE	LWF	06/12/2018
B	ADD C10005-006	LWF	06/27/2018

ITEM	PART NUMBER	DESCRIPTION	QTY
5	C10005-006	PVC GASKTE T=1.5mm	1
4	B50033-001	T-BOLT, RAIL BOTTOM SLOT, 3/8-16 X 1"	2
3	B20018-002	GROUNDING PIN	1
2	B15003-001	FLANGE NUT 3/8-16	2
1	A20329-001	2.5" AL PIPE U-BOLT	1

MATERIAL		SEE NOTES	
Third Angle Projection:			
SunModo Corp. 14800 NE 65TH STREET, VANCOUVER WA 98682			
GENERAL SPECIFICATIONS		TITLE	
All Dimensions in inches [millimeters] Tolerances X.XXX ±0.01 [0.25mm] X.XX ±0.02 [0.50mm] X.X ±0.039 [1.0mm] Unless otherwise spec'd		2.5" AL PIPE U-CLAMP KIT	
DRAWN BY		DATE	
KYY		06/12/2018	
CHECKED BY		DRAWING NUMBER	
		B K10343-001	
APPROVALS		SCALE: NONE	
		SHEET 1 of 1	

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REVISIONS			
REV	DESCRIPTION	BY	DATE
A	INITIAL RELEASE	zcg	09/25/2015

ITEM	PART NUMBER	DESCRIPTION	QTY
7	B10001-002	SET SCREW M10X10	2
6	B15048-001	STAR WASHER FOR 3/8 BOLT	1
5	B15018-004	HEX CAP SCREW 3/8-16 X2.5	1
4	B15003-001	FLANGE NUT 3/8-16	2
3	B15018-002	HEX CAP SCREW 3/8-16 X 1.25	1
2	A20239-001	2.5 AL PIPE CLAMP, FEMALE	1
1	A20238-001	2.5 AL PIPE CLAMP, MALE	1

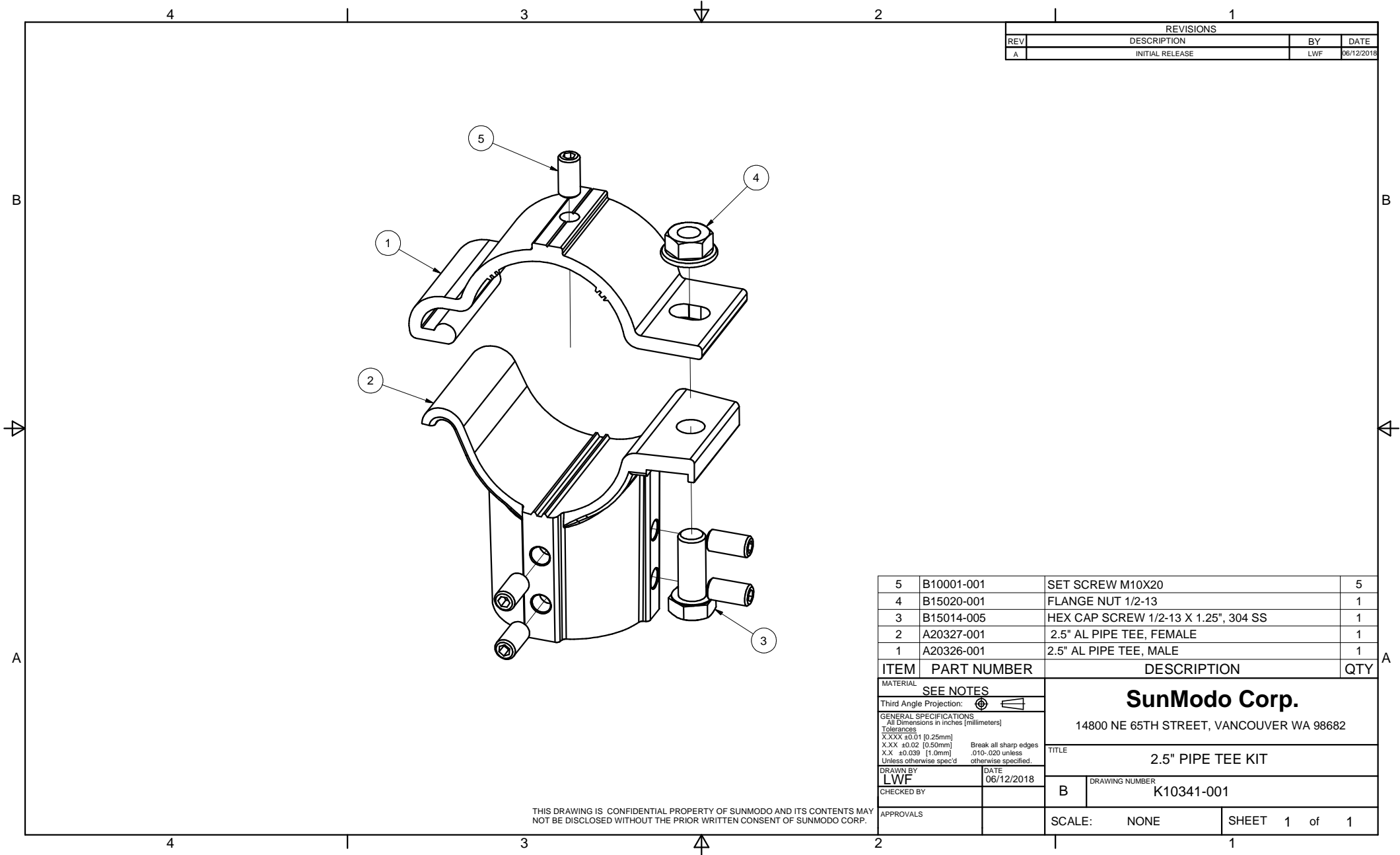
MATERIAL		SEE BOM	
Third Angle Projection:			
GENERAL SPECIFICATIONS All Dimensions in inches [millimeters] Tolerances X.XX ±0.01 (0.25mm) X.X ±0.02 (0.5mm) X.X ±0.03 (0.75mm) Unless otherwise specified.			
DRAWN BY		DATE	
LWF		08/21/2015	
CHECKED BY		B	
APPROVALS		SCALE: NONE	
		SHEET 1 of 1	

Sunmodo Corp.
 1905 E 5TH STREET, STE A, VANCOUVER, WA 98661

TITLE
2.5 AL PIPE CLAMP KIT

DRAWING NUMBER
K10222-001

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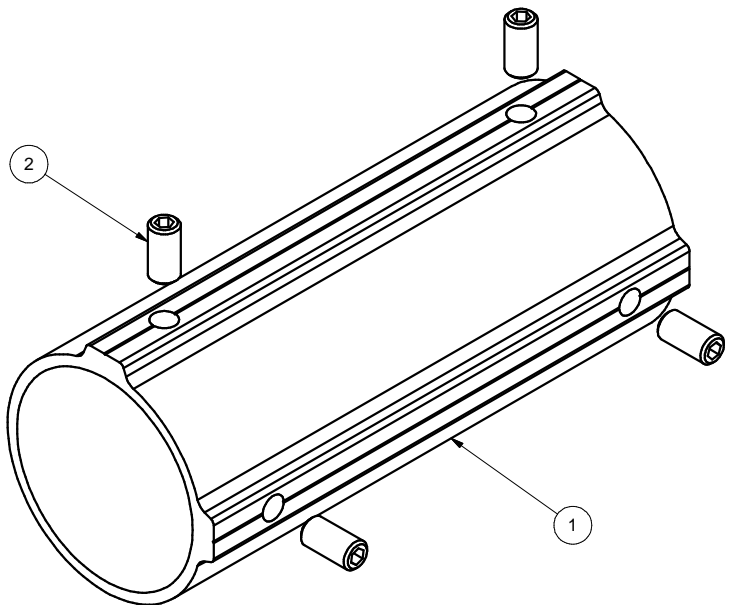
REVISIONS			
REV	DESCRIPTION	BY	DATE
A	INITIAL RELEASE	LWF	06/12/2018

ITEM	PART NUMBER	DESCRIPTION	QTY
5	B10001-001	SET SCREW M10X20	5
4	B15020-001	FLANGE NUT 1/2-13	1
3	B15014-005	HEX CAP SCREW 1/2-13 X 1.25", 304 SS	1
2	A20327-001	2.5" AL PIPE TEE, FEMALE	1
1	A20326-001	2.5" AL PIPE TEE, MALE	1

MATERIAL		SEE NOTES	
Third Angle Projection:			
GENERAL SPECIFICATIONS		SunModo Corp. 14800 NE 65TH STREET, VANCOUVER WA 98682	
Tolerances		TITLE	
X.XXX ±0.01 [0.25mm] X.XX ±0.02 [0.50mm] X.X ±0.039 [1.0mm] Unless otherwise spec'd		2.5" PIPE TEE KIT	
DRAWN BY		DATE	
LWF		06/12/2018	
CHECKED BY		DRAWING NUMBER	
		B K10341-001	
APPROVALS		SCALE: NONE SHEET 1 of 1	

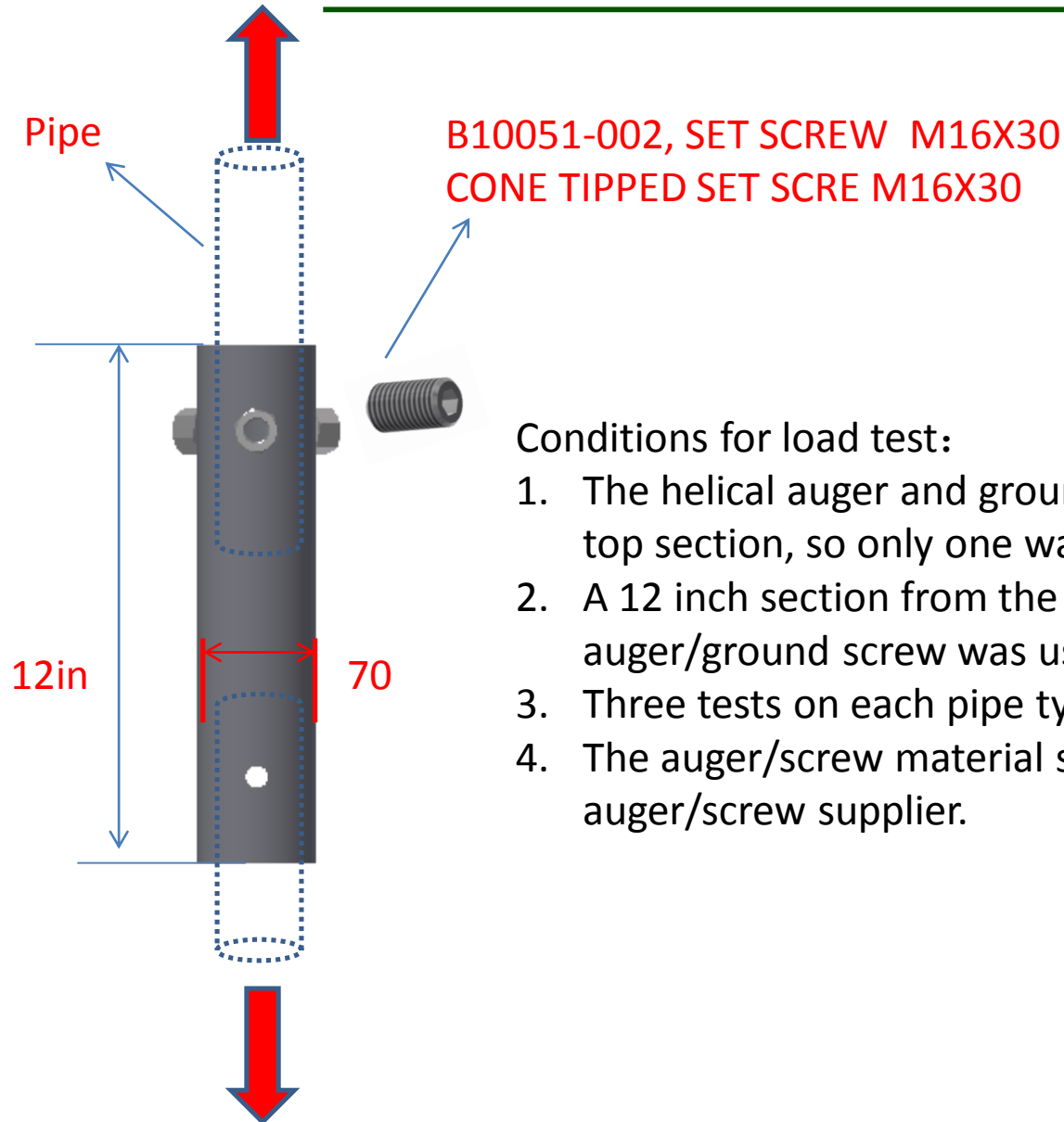
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REVISIONS			
REV	DESCRIPTION	BY	DATE
A	INITIAL RELEASE	LWF	06/12/2018



2	B10001-001	SET SCREW M10X20	4
1	A20328-001	2.5" PIPE SPLICE	1
ITEM	PART NUMBER	DESCRIPTION	QTY
MATERIAL		SEE NOTES	
Third Angle Projection:			
GENERAL SPECIFICATIONS		SunModo Corp. 14800 NE 65TH STREET, VANCOUVER WA 98682	
All Dimensions in inches [millimeters] Tolerances X.XXX ±0.01 [0.25mm] X.XX ±0.02 [0.50mm] X.X ±0.039 [1.0mm] Unless otherwise spec'd		Break all sharp edges .010-.020 unless otherwise specified.	
DRAWN BY		TITLE	
LWF		2.5" PIPE SPLICE KIT	
CHECKED BY		DRAWING NUMBER	
		B K10342-001	
APPROVALS		SCALE: NONE SHEET 1 of 1	

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Conditions for load test:

1. The helical auger and ground screw use the same top section, so only one was used for testing
2. A 12 inch section from the top of the auger/ground screw was used
3. Three tests on each pipe type was used
4. The auger/screw material supplied by the auger/screw supplier.